

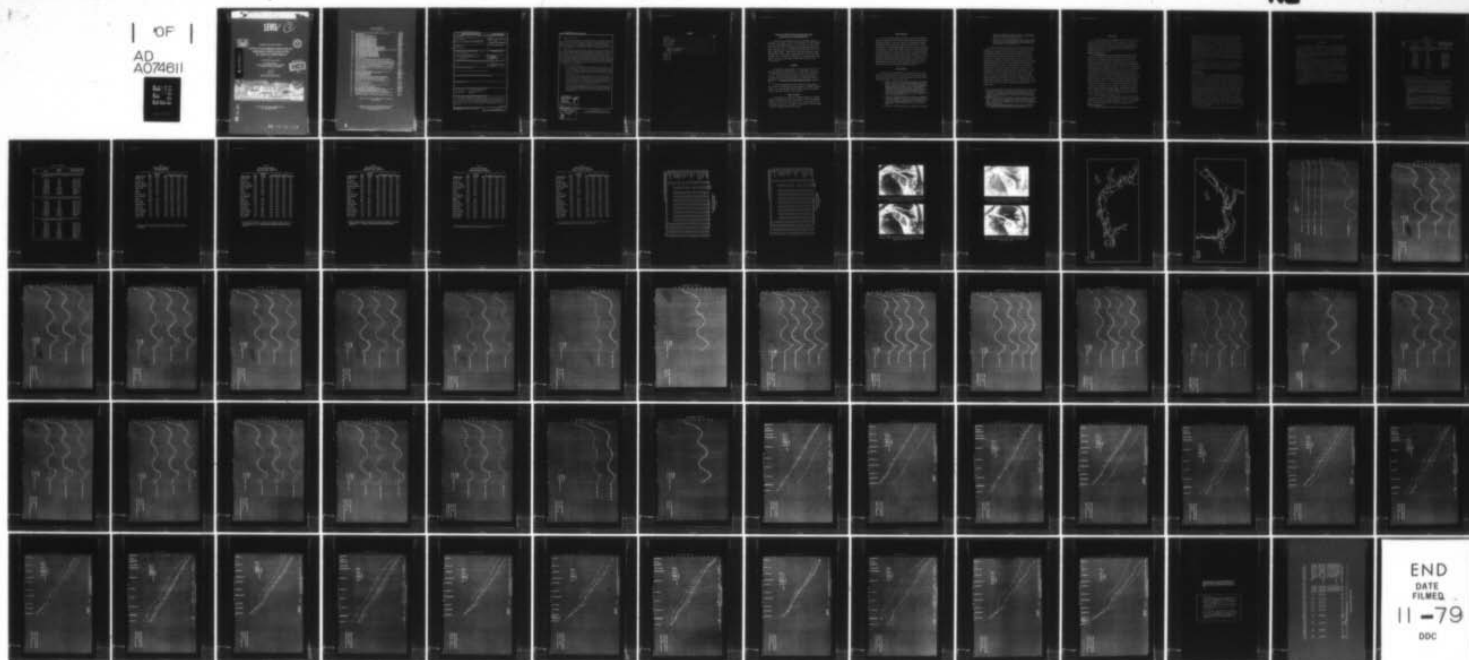
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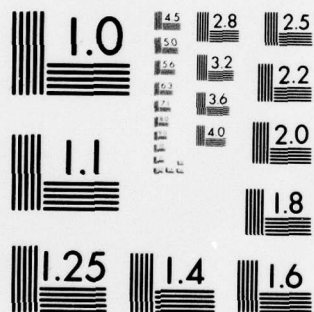
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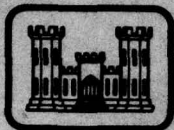
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MISSISSIPPI BASIN MODEL REPORT 81-6

**EFFECTS OF OVERBANK VEGETATION ON
MISSISSIPPI RIVER STAGES IN THE
ST. LOUIS-TO-THEBES REACH**

by

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June 1979

Final Report

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MISSISSIPPI BASIN MODEL REPORTS
Issued Prior to and Including This Report

Report No.	Title	Date
1-1	Preliminary Report on Proposed Reservoir Operation Model, Mississippi River and Tributaries	October 1941
1-2	Report on Proposed Site	October 1942
1-3	Definitive Project Report	April 1943
1-4	Description of the Mississippi Basin Model	July 1951
1-5	Automatic Interconnection of the Mississippi Basin Model	December 1955
1-6	History and Description of the Mississippi Basin Model	August 1971
2-1	Report of First Meeting of Mississippi Basin Model Board	October 1945
2-2	Report of Second Meeting of Mississippi Basin Model Board	March 1947
2-3	Report of Third Meeting of Mississippi Basin Model Board	May 1948
2-4	Report of Fourth Meeting of Mississippi Basin Model Board	August 1949
2-5	Report of Fifth Meeting of Mississippi Basin Model Board	June 1949
2-6	Report of Sixth Meeting of Mississippi Basin Model Board	March 1950
2-7	Report of Seventh Meeting of Mississippi Basin Model Board	March 1951
2-8	Report of Eighth Meeting of Mississippi Basin Model Board	August 1952
2-9	Report of Ninth Meeting of Mississippi Basin Model Board	September 1953
2-10	Report of Tenth Meeting of Mississippi Basin Model Board	October 1954
2-11	Report of Eleventh Meeting of Mississippi Basin Model Board	October 1954
2-12	Report of Twelfth Meeting of Mississippi Basin Model Board	May 1956
2-13	Report of Thirteenth (Fiscal Year 1957) Meeting of Mississippi Basin Model Board	May 1957
2-14	Report of Fourteenth (Fiscal Year 1958) Meeting of Mississippi Basin Model Board	May 1958
2-15	Report of Fifteenth (Fiscal Year 1959) Meeting of Mississippi Basin Model Board	May 1959
2-16	Report of Sixteenth Meeting of Mississippi Basin Model Board, Fiscal Year 1960	June 1960
2-17	Special Report of the Mississippi Basin Model on Curtailment of Model Limits (Seventeenth Meeting of the Board)	September 1960
2-18	Report of Eighteenth Meeting of Mississippi Basin Model Board, Fiscal Year 1961	July 1961
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2-26	Report of Twenty-Sixth Meeting of Mississippi Basin Model Board	June 1969
2-27	Report of Twenty-Seventh Meeting of Mississippi Basin Model Board	June 1970
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12-1	Verification of Sioux City-to-Burns Reach, Missouri River and Tributaries, 1930 and 1947 Floods	April 1952
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13-1	Verification of the Fishwick Run-Kentucky Run Reach, Tennessee River and Tributaries, 1950 and 1948 Floods	December 1960
14-1	Verification of Tulsa-to-Van Buren Reach, Arkansas River and Tributaries, Spring 1941 and 1943 Floods	July 1951
14-2	Verification of Van Buren-to-Pine Bluff Reach, Arkansas River and Tributaries, Spring 1941 and 1943 Floods	November 1952
15-1	Verification of Hannibal-to-St. Louis Reach, Mississippi River and Tributaries, 1947, 1944, and 1943 Floods	August 1951
15-2	Verification of Hannibal-to-Thobee Reach, Mississippi River and Tributaries, 1947, 1944, and 1943 Floods	May 1952
12-1	Effects of Reservoirs and Results of Steady-Flow Tests, Cumberland River	June 1965
12-2	Kentucky Reservoir Steady Flow Profiles and Effects of Fishwick Discharge Duration on Downstream Stages	July 1965
12-3	Effects of Cheatham and Barkley Reservoirs and Coordinated Operation of Barkley and Kentucky Reservoirs, Cumberland and Tennessee Rivers	May 1969
24-1	Flood-Warning and Reservoir-Operation Study, Tulsa-to-Van Buren Reach, Arkansas River and Tributaries	April 1961
29-1	Comprehensive Testing Program	November 1971
31-1	Operation of the Birds Point-New Madrid Floodway	July 1957
31-2	Adequacy of Project Levee Grades in Hannibal-to-Thobee Reach, Mississippi River and Tributaries	April 1957
31-3	Proposed Alignment for Columbia Bottom Levee, St. Louis Industrial Park	January 1960
31-4	Mississippi River Hypothetical Flood 525	September 1962
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31-7	Tests of Birds Point-New Madrid Floodway	March 1978
32-1	Effects of Agricultural Levees on Design Flood Profiles for Hannan City Local Protection	May 1955
32-2	Tests for Re-evaluation of Missouri River Agricultural Levees in the Hannan City District	December 1959
32-3	Tests for Re-evaluation of Missouri River Agricultural Levees in the Omaha District	May 1960
34-1	Effects of Project Levees Along Point Barrow Creek, Tributary of Arkansas River	June 1954
34-2	Adequacy of Project Levee Grades Without and with Reservoir Modification, Van Buren to Pine Bluff, Arkansas River	April 1957
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42-1	Hypothetical Storms over the Iowa Tributaries	October 1956
43-1	The Ohio River Hypothetical Flood 60-1	February 1963
44-1	Determination of Discharge Hydrographs for Arkansas River and Tributaries, April 1927 Flood	June 1956
52-1	Tests of Channel Realignment near St. Joseph, Missouri	October 1954
61-1	Effects of Proposed Highway Fill Across Cheatham Island	January 1959
61-2	Effects of Proposed Chain of Banks Run, Mississippi River, Mile 150.1	September 1959
61-3	Effects of Highway Construction on Mississippi River Flow, Lake County, Tennessee	December 1967
61-4	Report of Model Study, Effects of Modifying Operation of Old River Control Structures on 1945, 1941, 1947, and 1948 Flood Flows; Appendix A, Additional Hydrographs	March 1972
66-1	Report of Model Study Effects of Ultimate Channel Development in the Atchafalaya Basin	December 1973
61-4	Effects of Overbank Vegetation on Mississippi River Stages in the St. Louis-to-Thobee Reach	June 1979
66-1	Effects of Roadway Encroachment and Waterway Opening of Proposed Interstate Highway 155 on Mississippi River Floods	July 1966
66-2	Effects of Southend Maritime Centre on Ohio River Flow Conditions at Mount Vernon, Indiana	April 1972
92-1	Effects of Flood Heights of Levee, Railroad, and Highway Fills in the Flood Plain of the Missouri River	October 1953

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) → This model investigation was conducted on the St. Louis-to-Commerce Reach of the Mississippi Basin Model to determine stages to be expected along the Mississippi River with varying amounts of overbank vegetation between the river and its bluff line or levee. The data obtained from this study will be used to determine the sensitivity of the flow regime to land-use changes riverside of the levees. (Continued)		

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20. ABSTRACT (Continued).

The Mississippi Basin Model is a fixed-bed model of the Mississippi River and its tributary system built to a horizontal scale of 1:2000 and a vertical scale of 1:100. Prior to conducting this study, the model was adjusted to reproduce the 1973 flood. The overbank roughness was placed on the model at locations where aerial photographs showed timber to exist in the prototype in 1973. The density of this roughness was adjusted to reproduce prototype stages for the 1973 flood.

Four series of tests were conducted in this study. Each series simulated a different overbank vegetation condition between the river and its bluff line. For Series I, folded screen wire was installed on all areas between the river and its bluff line or levee to a density that simulated the effect of the overbank vegetation fully developed in its natural state. For Series II, folded screen wire was installed to the same density used for Series I only on overbank areas where vegetation existed in 1973. For Series III, folded screen wire was installed where overbank vegetation existed in 1973 to the density required to reproduce 1973 flood stages. For Series IV, folded screen wire was removed from overbank areas. Hydrograph flows of the 1973 flood and six steady flows were tested in each series of tests.

Test results indicate that:

- a. If the existing overbank vegetation were allowed to develop fully in its natural state, the stages in the test reach would increase as much as 1.7 ft for the flows tested. This increase in density would cause a flow of 1,000,000 cfs, which would be essentially contained by 1973 levees with existing overbank vegetation, to overtop 1973 levee grades by as much as 1.1 ft.
- b. If the vegetation were allowed to develop fully in its natural state over the entire overbank area from the river to its levee or bluff line, stages in the test reach would be increased by as much as 3.7 ft for the flows tested. This increase in area and density of overbank vegetation would cause a 1,000,000-cfs flow to overtop 1973 levee grades by as much as 1.6 ft. The 1973 levees would have to be raised 3.5 ft to contain this flow with this condition.
- c. If the existing overbank vegetation were to be removed, stages in the test reach would be lowered by as much as 7.6 ft. With the overbank vegetation removed, all flows tested would be contained by the 1973 levees except the 1,300,000-cfs flow near Grand Tower and downstream of Devils Island.

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EFFECTS OF OVBANK VEGETATION ON MISSISSIPPI RIVER
STAGES IN THE ST. LOUIS-TO-THEBES REACH

1. Model tests to determine the effects of overbank vegetation on Mississippi River stages in the St. Louis-to-Thebes reach were requested by the U. S. Army Engineer District, St. Louis (LMS), in letter dated 4 October 1977 to the U. S. Army Engineer Waterways Experiment Station (WES). Additional tests were requested during subsequent visits to the model by LMS personnel. Funds for the study were authorized in Intra-Army Orders No. ED 78-1, dated 4 October 1977 and No. ED 78-1R1, dated 30 August 1978. The study was conducted on the Mississippi Basin Model (MBM) at the Jackson Installation of WES during the period 8 June-11 October 1978.

The Model

2. The MBM is a fixed-bed model of the Mississippi River and its tributary system from Hannibal, Missouri, to Baton Rouge, Louisiana. It is constructed to a horizontal scale of 1:2000 and a vertical scale of 1:100. General features of this model, including appurtenances, instrumentation, and operating procedures, are described in detail in MBM Report 1-4, Description of the Mississippi Basin Model, dated July 1951.

3. The study reported herein was conducted on the Mississippi River portion of the MBM from St. Louis, Missouri, to Commerce, Missouri. Plates 1 and 2 show the model limits, streams, inflow points, gaging stations, and levee locations in the test reach.

Purpose of Study

4. These tests were conducted to determine stages to be expected along the Mississippi River with varying amounts of overbank vegetation between the river and its bluff line or levee. The data obtained from these tests will be used to determine the sensitivity of the flow regime to land-use changes riverside of the levees.

Model Adjustment

5. Prior to conducting this study, the test reach of the MBM was adjusted to reproduce the 1973 flood to ensure that the model reflected existing conditions. Levees were installed to alignments and grades furnished by the LMS the same as those that existed in 1973. Folded screen wire, cut to the average height of trees in the area, was placed on the model in locations where timber was shown on infrared photographs that were taken in 1973. Flows that occurred in the prototype during the period 3 March to 8 May 1973 (Plate 3) were introduced at model inflow points and routed to Grays Point, Missouri, where the water surface was held to elevations recorded in the prototype. The density of the screen wire and the length and spacing of channel roughness elements were adjusted until the model stage hydrographs agreed closely with those that occurred in the prototype during this period.

Test Procedure

6. Four series of tests (Table 1) were conducted in this study. Each series simulated different overbank vegetation conditions between the river and its bluff line or levee from Columbia Drainage and Levee District (mile 167) to Grays Point (mile 45).

- a. Series I - Folded screen wire was installed to the density shown in Photo 1 on all overbank areas between the river and its levee or bluff line. This condition simulated the effect of overbank vegetation on the entire overbank area developed fully in its natural state. The density of screen wire to simulate this natural prototype state was determined from that required for adjustment of that portion of the model simulating areas of the Atchafalaya Basin where the overbank vegetation has developed naturally, over a long period of time.
- b. Series II - Folded screen wire was installed on overbank areas where vegetation existed in 1973 to the density used in Series I (Photo 2). This condition simulated the effect of the overbank vegetation on only the areas covered by existing vegetation developed fully in its natural state.
- c. Series III - Folded screen wire was installed on overbank

areas where vegetation existed in 1973 to the density required to reproduce 1973 stages (Photo 3). This condition simulated existing prototype conditions.

- d. Series IV - All folded screen wire between the river and its bluff line or levee was removed. This condition simulates the effect of completely clearing the vegetation in the area along the river (Photo 4).

7. Eleven tests were conducted in each series using seven flows: prototype flows for the period 3 March-8 May 1973 (same as flows used for adjustment and shown in Plate 3) and six steady flows--600,000, 700,000, 872,000,* 889,000,** 1,000,000, and 1,300,000 cfs. These seven flows were introduced into the model and routed to Grays Point with levees to alignment and grade existing in 1973. Water-surface elevations at Grays Point were held to prototype stages for the period 3 March-8 May 1973; to the crest of the 1973 flood for steady flows of 872,000 and 889,000 cfs; and to a rating curve† for the remaining steady flows. Two of these flows, 1,000,000 and 1,300,000 cfs, were reintroduced and routed to Grays Point with the levees raised to confining grade. The water surface at Grays Point was held to the same elevation as for the corresponding flow with levees to 1973 grade. These two flows were reintroduced and routed to Commerce (7.0 miles downstream from Grays Point) with the levees to confining grade. The water-surface elevation at Commerce was held to a rating curve.† Water-surface elevations were recorded at model gaging stations shown in Plates 1 and 2.

* Steady flow of 872,000 cfs reproduced crest stages of the 1973 flood. It consisted of 844,000 cfs on the Mississippi River at St. Louis; 11,000 cfs on the Meramec River; 8,000 cfs on the Kaskaskia River; 7,000 cfs on the Big Muddy River; and 2,000 cfs on the Little River Diversion Canal.

** Steady flow of 889,000 cfs simulated the crest discharge of the 1973 flood. It consisted of 850,000 cfs on the Mississippi River at St. Louis; 15,000 cfs on the Meramec River; 12,000 cfs on the Kaskaskia River; 10,000 cfs on the Big Muddy River; and 2,000 cfs on the Little River Diversion Canal.

† Rating curve was developed from model test results in MBM Report 31-5, Flowline Study, Mississippi and Illinois Rivers, June 1977.

Test Results

8. The stage and discharge hydrographs recorded for the four series of tests with 1973 flood flows are shown in Plates 4-25. The crest elevations are presented in Table 2. The water-surface elevations recorded for the four series of tests with the various steady flows are presented in Tables 3-8. These elevations are presented as water-surface profiles in Plates 26-43.

Series II vs Series III

9. Increasing the density of the overbank vegetation from that existing in 1973 raised the Mississippi River stages for all flows tested with the maximum increase for each flow in the vicinity of Brickeys and Little Rock Landing. The maximum increase in stages for flows of 600,000 and 700,000 cfs was only 0.3 and 0.6 ft, respectively; but for flows of the magnitude of the 1973 flood (872,000 cfs and above) the maximum increase in stages was from 1.4 to 1.7 ft. The increases in crest stages of the hydrograph flows were about the same as those for the steady flows simulating the crest stages (872,000 cfs) and discharges (889,000 cfs). With 1973 vegetation, the flow of 1,000,000 cfs overtopped the 1973 levee grades only at Waters Point and by only 0.1 ft. With this flow, increasing the density of overbank vegetation raised stages at Waters Point by 1.0 ft and caused the 1973 levees at Waters Point to be overtopped by 1.1 ft. With 1973 vegetation, the flow of 1,300,000 cfs overtopped 1973 levee grades in the entire test reach except for the area near Little Rock Landing. Increasing the density of the overbank vegetation increased stages for the flow of 1,300,000 cfs by as much as 1.7 ft (at Little Rock Landing) and caused the 1973 levees to be overtopped by as much as 3.3 ft.

10. Confining levee tests indicated that if the 1973 levees were high enough to contain the flows, increasing the density of the overbank vegetation would increase stages as much as 1.4 and 1.5 ft (at Waters Point) for flows of 1,000,000 and 1,300,000 cfs, respectively.

Series I vs Series III

11. Increasing the area and density of overbank vegetation from

that existing in 1973 raised Mississippi River stages for all flows tested with the maximum increase for the 600,000-cfs flow at Moccasin Springs and for all other flows tested at Little Rock Landing. The maximum increase was 0.9 ft for the 600,000-cfs flow, 1.6 ft for the 700,000-cfs flow, and from 3.4 to 3.7 ft for the remaining flows tested. Increasing the area and density of overbank vegetation with 1973 levees increased stages for 1,000,000 cfs to the point that the 1973 levee grades were exceeded up to 1.6 ft from Waters Point to Crawford Landing except for the area at Little Rock Landing. Increasing the area and density of the overbank vegetation with 1973 levees increased stages for 1,300,000 cfs to the point that 1973 levee grades were exceeded by as much as 4.0 ft.

12. Confining levee tests indicated that if the 1973 levees were high enough to contain the flows, increasing the area and density of overbank vegetation would increase stages as much as 4.6 and 6.2 ft (at Little Rock Landing) for flows of 1,000,000 and 1,300,000 cfs, respectively.

Series III vs IV

13. Clearing all of the overbank vegetation that existed in the area along the river in 1973 reduced Mississippi River stages throughout the test reach. The maximum reduction occurred at Waters Point for all flows except the 1,300,000 cfs; for this flow, the maximum reduction was at Brickeys. The maximum reduction with 1973 levees was from 1.9 ft for 600,000 cfs to 7.6 ft for 1,000,000 cfs. With no overbank vegetation, the only flow that overtopped the 1973 levees was 1,300,000 cfs which overtopped them only near Grand Tower and from Devils Island to Grays Point. Maximum overtopping was 3.3 ft at Grays Point. Part of this overtopping was because the Grays Point stages were held to the same elevation for all four series of tests. Test results indicate that holding stages at Commerce instead of at Grays Point would lower Grays Point stages about 2 ft, but would have little effect on the differences in stages caused by changing the density and location of overbank roughness upstream of Grays Point.

14. Confining levee tests indicated that if the 1973 levees were

high enough to contain the 1,300,000-cfs flow, clearing the overbank vegetation would reduce stages as much as 13.1 ft (at Waters Point).

Conclusions

15. If the existing overbank vegetation were allowed to develop fully in its natural state, the stages in the test reach would increase as much as 1.7 ft for the flows tested. This increase in density would cause a flow of 1,000,000 cfs, which would be essentially contained by 1973 levees with existing overbank vegetation, to overtop 1973 levee grades by as much as 1.1 ft.

16. If the vegetation were allowed to develop fully in its natural state over the entire overbank area from the river to its levee or bluff line, stages in the test reach would be increased by as much as 3.7 ft for the flows tested. This increase in area and density of overbank vegetation would cause a 1,000,000-cfs flow to overtop 1973 levee grades by as much as 1.6 ft. The 1973 levees would have to be raised 3.5 ft to contain this flow with this condition.

17. If the existing overbank vegetation were to be removed, stages in the test reach would be lowered by as much as 7.6 ft. With the overbank vegetation removed, all flows tested would be contained by the 1973 levees except the 1,300,000-cfs flow near Grand Tower and downstream of Devils Island.

Table 1
Test Conditions

Test No.	Flow*	Levee Grades	Water-Surface Elevation Controlled At
Series I - Overbank roughness simulating vegetation fully developed in its natural state on all overbank areas between channel and corresponding levee or high bank.			
1	1973 Hyd	1973	Grays Point
2	600,000	1973	Grays Point
3	700,000	1973	Grays Point
4	872,000	1973	Grays Point
5	889,000	1973	Grays Point
6	1,000,000	1973	Grays Point
7	1,000,000	Confined	Grays Point
8	1,000,000	Confined	Commerce
9	1,300,000	1973	Grays Point
10	1,300,000	Confined	Grays Point
11	1,300,000	Confined	Commerce

(Continued)

* Flows for tests were as follows:

- a. Tests 1, 12, 23, and 34 - flows that occurred in the prototype during the period 3 March to 8 May 1973 were used. These flows were used in adjustment tests and are shown in Plate 3.
- b. Tests 4, 15, 26, and 37 - steady flows reproducing crest stages of the 1973 flood were used. The total flow passing Grays Point was 872,000 cfs. It consisted of 844,000 cfs on the Mississippi River at St. Louis, Missouri; 11,000 cfs on the Meramec River; 8,000 cfs on the Kaskaskia River; 7,000 cfs on the Big Muddy River; and 2,000 cfs on the Little River Diversion Canal.
- c. Test 5, 16, 27, and 38 - steady flows simulating the crest discharges of the 1973 flood were used. 889,000 cfs was the total flow passing Grays Point. It consisted of 850,000 cfs on the Mississippi River at St. Louis, Missouri; 15,000 cfs on the Meramec River; 12,000 cfs on the Kaskaskia River; 10,000 cfs on the Big Muddy River; and 2,000 cfs on the Little River Diversion Canal.
- d. For all other tests, the total steady flow listed was introduced on the Mississippi River at St. Louis, Missouri.

Table 1 (Continued)

Test No.	Flow	Levee Grades	Water-Surface Elevation Controlled At
Series II - Overbank roughness simulating vegetation fully developed in its natural state only on overbank areas where vegetation existed in 1973.			
12	1973 Hyd	1973	Grays Point
13	600,000	1973	Grays Point
14	700,000	1973	Grays Point
15	872,000	1973	Grays Point
16	889,000	1973	Grays Point
17	1,000,000	1973	Grays Point
18	1,000,000	Confined	Grays Point
19	1,000,000	Confined	Commerce
20	1,300,000	1973	Grays Point
21	1,300,000	Confined	Grays Point
22	1,300,000	Confined	Commerce
Series III - Overbank roughness on areas where vegetation existed in 1973 to density required to reproduce 1973 flood stages.			
23	1973 Hyd	1973	Grays Point
24	600,000	1973	Grays Point
25	700,000	1973	Grays Point
26	872,000	1973	Grays Point
27	889,000	1973	Grays Point
28	1,000,000	1973	Grays Point
29	1,000,000	Confined	Grays Point
30	1,000,000	Confined	Commerce
31	1,300,000	1973	Grays Point
32	1,300,000	Confined	Grays Point
33	1,300,000	Confined	Commerce
Series IV - All overbank roughness removed between channel and corresponding levee or high bank.			
34	1973 Hyd	1973	Grays Point
35	600,000	1973	Grays Point
36	700,000	1973	Grays Point
37	872,000	1973	Grays Point
38	889,000	1973	Grays Point
39	1,000,000	1973	Grays Point
40	1,000,000	Confined	Grays Point
41	1,000,000	Confined	Commerce
42	1,300,000	1973	Grays Point
43	1,300,000	Confined	Grays Point
44	1,300,000	Confined	Commerce

Table 2
Water-Surface Elevations
1973 Hydrograph Tests

Gaging Station	River Mile	Existing Levee El ft msl	Water-Surface El, ft msl			
			Test 1	Test 12	Test 23	Test 34
Bissell Point	183.3	436.4	426.3	425.2	424.6	422.8
St. Louis	179.6	433.6	424.5	423.4	422.8	420.2
Engineer Depot	176.8	430.7	422.2	420.9	420.2	417.3
Mo. Pac. Elevator	172.6	425.5	420.3	418.9	417.9	414.6
Jefferson Barracks	169.3	424.2	418.8	417.0	416.4	412.1
Waters Point	158.5	415.4	413.2	411.9	410.6	405.4
Selma	146.0	409.5	406.8	405.2	403.9	399.4
Brickeys	136.0	405.2	401.1	399.4	398.4	395.4
Little Rock Ldg.	125.5	399.5	394.4	392.4	390.9	387.1
East Kaskaskia	116.2		389.7	388.6	388.2	384.1
Chester	109.5	390.0	385.9	384.6	384.1	379.5
Bishop Ldg.	100.8	385.4	381.6	379.6	379.0	375.4
Red Rock Ldg.	94.1	381.7	378.5	376.9	376.5	372.6
Cumberland Rock	87.0	377.2	373.9	372.1	371.9	368.3
Grand Tower	81.0	373.1	370.3	369.4	368.9	365.4
Crawford Ldg.	72.9	368.3	364.1	362.6	362.0	358.7
Moccasin Springs	66.3	364.6	360.2	358.8	358.0	354.7
Devils Island	57.3	360.3	356.4	355.4	355.2	353.4
Cape Girardeau	52.1	356.4	351.5	350.8	350.4	349.4
Grays Point*	46.3	350.4	345.8	345.8	345.8	345.8

* Water surface at Grays Point held to that recorded in the prototype during 1973 flood.

Table 3
Water-Surface Elevations
Steady Flow Tests - 600,000 cfs

<u>Gaging Station</u>	<u>River Mile</u>	<u>Existing Levee El ft msl</u>	<u>Water-Surface El, ft msl</u>			
			<u>Test 2</u>	<u>Test 13</u>	<u>Test 24</u>	<u>Test 35</u>
Bissell Point	183.3	436.4	416.3	415.9	415.9	415.3
St. Louis	179.6	433.6	414.4	414.0	414.0	413.1
Engineer Depot	176.8	430.7	412.4	412.0	412.0	411.0
Mo. Pac. Elevator	172.6	425.5	410.4	409.5	409.5	408.6
Jefferson Barracks	169.3	424.2	408.6	408.1	408.1	406.6
Waters Point	158.5	415.4	403.2	402.6	402.4	400.5
Selma	146.0	409.5	396.6	396.2	396.0	394.2
Brickeys	136.0	405.2	391.4	391.1	390.8	389.5
Little Rock Ldg.	125.5	399.5	385.0	384.4	384.4	383.3
East Kaskaskia	116.2		379.3	378.7	378.7	378.0
Chester	109.5	390.0	375.5	375.0	375.0	373.9
Bishop Ldg.	100.8	385.4	370.8	370.2	370.2	369.4
Red Rock Ldg.	94.1	381.7	367.4	366.7	366.7	365.5
Cumberland Rock	87.0	377.2	363.2	362.5	362.5	361.1
Grand Tower	81.0	373.1	360.3	359.6	359.5	358.4
Crawford Ldg.	72.9	368.3	354.4	353.7	353.6	352.3
Moccasin Springs	66.3	364.6	350.7	350.1	349.8	348.4
Devils Island	57.3	360.3	346.9	346.4	346.4	345.9
Cape Girardeau	52.1	356.4	343.0	342.4	342.3	341.7
Grays Point*	46.3	350.4	338.0	338.0	338.0	338.0

* Water surface was held to a rating curve developed from model test results in MBM report 31-5, Flowline Study, Mississippi and Illinois Rivers, June 1977.

Table 4
Water-Surface Elevations
Steady Flow Tests - 700,000 cfs

<u>Gaging Station</u>	<u>River Mile</u>	<u>Existing Levee El ft msl</u>	<u>Water-Surface El, ft msl</u>			
			<u>Test 3</u>	<u>Test 14</u>	<u>Test 25</u>	<u>Test 36</u>
Bissell Point	183.3	436.4	420.3	419.6	419.6	418.6
St. Louis	179.6	433.6	418.3	417.6	417.6	416.3
Engineer Depot	176.8	430.7	416.2	415.3	415.3	413.7
Mo. Pac. Elevator	172.6	425.5	414.2	413.1	412.9	411.0
Jefferson Barracks	169.3	424.2	412.6	411.6	411.4	409.0
Waters Point	158.5	415.4	407.0	406.1	405.7	402.6
Selma	146.0	409.5	400.4	399.6	399.2	396.4
Brickeys	136.0	405.2	395.1	394.2	393.6	392.0
Little Rock Ldg.	125.5	399.5	388.5	387.3	386.9	385.1
East Kaskaskia	116.2		383.2	382.4	382.2	380.5
Chester	109.5	390.0	379.4	378.7	378.6	376.0
Bishop Ldg.	100.8	385.4	374.8	373.5	373.5	372.0
Red Rock Ldg.	94.1	381.7	371.6	370.8	370.7	368.2
Cumberland Rock	87.0	377.2	367.2	366.0	366.0	363.9
Grand Tower	81.0	373.1	363.9	363.1	362.9	360.9
Crawford Ldg.	72.9	368.3	358.0	357.0	356.8	354.5
Moccasin Springs	66.3	364.6	354.0	353.2	352.9	350.4
Devils Island	57.3	360.3	350.2	349.7	349.6	348.5
Cape Girardeau	52.1	356.4	345.9	345.3	345.1	344.6
Grays Point*	46.3	350.4	340.7	340.7	340.7	340.7

* Water surface was held to a rating curve developed from model test results in MBM Report 31-5, Flowline Study, Mississippi and Illinois Rivers, June 1977.

Table 5
Water-Surface Elevations
Steady Flow Tests - 872,000 cfs

<u>Gaging Station</u>	<u>River Mile</u>	<u>Existing Levee El ft msl</u>	<u>Water-Surface El, ft msl</u>			
			<u>Test 4</u>	<u>Test 15</u>	<u>Test 26</u>	<u>Test 37</u>
Bissell Point	183.3	436.4	426.6	425.5	424.7	422.7
St. Louis	179.6	433.6	424.5	423.4	422.6	420.2
Engineer Depot	176.8	430.7	422.3	421.0	420.2	417.2
Mo. Pac. Elevator	172.6	425.5	420.4	418.6	417.8	414.4
Jefferson Barracks	169.3	424.2	419.1	417.3	416.4	412.1
Waters Point	158.5	415.4	413.4	412.1	410.8	405.5
Selma	146.0	409.5	406.9	405.3	404.0	399.3
Brickeys	136.0	405.2	401.4	399.7	398.4	395.2
Little Rock Ldg.	125.5	399.5	394.7	392.6	391.2	387.0
East Kaskaskia	116.2		390.1	388.7	388.2	383.9
Chester	109.5	390.0	386.4	384.7	384.1	379.3
Bishop Ldg.	100.8	385.4	382.1	379.7	379.1	375.2
Red Rock Ldg.	94.1	381.7	378.8	377.1	376.5	372.4
Cumberland Rock	87.0	377.2	374.4	372.3	371.9	368.1
Grand Tower	81.0	373.1	370.6	369.4	369.0	365.4
Crawford Ldg.	72.9	368.3	364.5	362.8	362.1	358.6
Moccasin Springs	66.3	364.6	360.5	359.0	358.3	354.5
Devils Island	57.3	360.3	356.8	355.4	355.2	353.4
Cape Girardeau	52.1	356.4	351.6	350.7	350.6	349.4
Grays Point*	46.3	350.4	345.8	345.8	345.8	345.8

* Water surface controlled to the crest of the 1973 flood.

Table 6
Water-Surface Elevations
Steady Flow Tests ~ 889,000 cfs

<u>Gaging Station</u>	<u>River Mile</u>	<u>Existing Levee El ft msl</u>	<u>Water-Surface El, ft msl</u>			
			<u>Test 5</u>	<u>Test 16</u>	<u>Test 27</u>	<u>Test 38</u>
Bissell Point	183.3	436.4	426.9	425.9	425.1	422.8
St. Louis	179.6	433.6	424.9	423.8	423.0	420.5
Engineer Depot	176.8	430.7	422.7	421.3	420.6	417.4
Mo. Pac. Elevator	172.6	425.5	420.8	419.1	418.1	414.6
Jefferson Barracks	169.3	424.2	419.5	417.7	416.7	412.3
Waters Point	158.5	415.4	413.8	412.4	411.2	405.6
Selma	146.0	409.5	407.4	405.8	404.5	399.5
Brickeys	136.0	405.2	401.8	400.1	398.8	395.4
Little Rock Ldg.	125.5	399.5	395.3	393.0	391.6	387.2
East Kaskaskia	116.2		390.7	389.3	388.8	384.1
Chester	109.5	390.0	387.0	385.2	384.6	379.6
Bishop Ldg.	100.8	385.4	382.7	380.1	379.6	375.5
Red Rock Ldg.	94.1	381.7	379.4	377.6	377.0	372.8
Cumberland Rock	87.0	377.2	375.0	372.7	372.3	368.5
Grand Tower	81.0	373.1	371.2	369.9	369.4	365.7
Crawford Ldg.	72.9	368.3	365.0	363.2	362.6	359.0
Moccasin Springs	66.3	364.6	360.9	359.4	358.7	354.7
Devils Island	57.3	360.3	357.2	355.7	355.6	353.6
Cape Girardeau	52.1	356.4	351.8	350.9	350.8	349.6
Grays Point*	46.3	350.4	345.8	345.8	345.8	345.8

* Water surface controlled to the crest of the 1973 flood.

Table 7
Water-Surface Elevations
Steady-Flow Tests - 1,000,000 cfs

Gaging Station	River Mile	Existing Levee El ft msl	Water-Surface Elevations, ft msl, for Test Nos.											
			6	17	28	39	7	18	29	40	8	19	30	41
Blaneil Point	183.3	436.4	430.6	430.2	429.7	426.8	431.6	430.4	429.7	426.8	431.6	430.4	429.7	426.8
St. Louis	179.6	433.6	428.8	428.1	427.8	424.3	430.0	428.6	427.8	424.3	430.0	428.6	427.8	424.3
Engineer Depot	176.8	430.7	426.3	425.5	425.2	420.7	427.8	426.0	425.2	420.7	427.8	426.0	425.2	420.7
No. Pac. Elevator	172.6	425.5	424.1	423.1	422.5	417.4	425.7	423.9	422.8	417.4	425.7	423.9	422.8	417.4
Jefferson Barracks	169.3	424.2	422.5	421.6	421.1	414.9	424.6	422.4	421.3	414.9	424.6	422.4	421.3	414.9
Waters Point	158.5	415.4	417.0	416.5	415.5	407.9	418.9	417.1	415.7	407.9	418.9	417.1	415.7	407.9
Selma	146.0	409.5	410.7	409.6	408.6	401.8	412.3	409.9	408.6	401.8	412.3	409.9	408.6	401.8
Brickleys	136.0	405.2	405.4	403.8	402.5	397.8	406.4	403.8	402.6	397.8	406.4	403.8	402.5	397.8
Little Rock Ldg.	125.5	399.5	398.4	396.5	395.0	388.8	399.6	396.5	395.0	388.8	399.6	396.5	395.0	388.8
East Kaskaskia	116.2	390.0	393.7	393.2	392.5	386.5	395.3	393.2	392.5	386.5	395.3	393.2	392.5	386.5
Chester	109.5	390.0	390.2	388.9	388.4	382.2	391.5	388.9	388.4	382.2	391.5	388.9	388.4	382.2
Bishop Ldg.	100.8	385.4	386.5	383.9	383.2	377.9	387.5	383.9	383.2	377.9	387.5	383.9	383.2	377.9
Red Rock Ldg.	94.1	381.7	383.3	381.3	380.6	375.3	384.2	381.3	380.6	375.3	384.2	381.3	380.6	375.3
Cumberland Rock	87.0	377.2	378.4	376.1	375.6	371.2	379.4	376.1	375.6	371.2	379.4	376.1	375.6	371.2
Grand Tower	81.0	373.1	374.6	373.1	372.6	368.6	375.0	373.1	372.6	368.6	375.0	373.1	372.6	368.6
Crawford Ldg.	72.9	368.3	368.4	366.2	365.6	361.1	368.6	366.2	365.6	361.1	368.6	366.2	365.6	361.1
Moccasin Springs	66.3	364.6	364.1	362.3	361.7	356.7	364.1	362.3	361.7	356.7	364.1	362.3	361.7	356.7
Devils Island	57.3	360.3	360.3	358.4	358.3	355.7	360.3	358.4	358.3	355.7	360.3	358.4	358.3	355.7
Cape Girardeau	52.1	356.4	354.4	353.4	353.1	352.0	354.4	353.4	353.1	352.0	354.4	353.4	353.1	352.0
Greys Point*	46.3	350.4	347.6	347.6	347.6	347.6	347.6	347.6	347.6	347.6	347.6	347.6	347.6	347.6
Thebes	43.7													
Counterfeit Rock	42.3													
Commerce*	39.3													

* Water surface at Greys Point was held to a rating curve developed from model test results in NRM Report 31-5, Flow-Line Study, Mississippi and Illinois Rivers, June 1977.

Table 8
Water-Surface Elevations
Steady-Flow Tests - 1,300,000 cfs

Gaging Station	River Levee El ft msl	Water-Surface Elevations, ft msl, for Test Nos.															
		9	20	31	42	10	21	32	43	11	22	33	44				
Blasell Point	183.3	435.9	435.7	435.4	434.2	444.1	441.9	440.8	434.2	444.1	441.9	440.8	434.2				
St. Louis	179.6	433.8	433.6	433.3	431.9	441.0	438.6	437.6	431.9	441.0	438.6	437.6	431.9				
Engineer Depot	176.8	430.4	429.8	429.5	427.6	438.4	435.7	434.7	427.6	438.4	435.7	434.7	427.6				
Mo. Pac. Elevator	172.6	425.5	427.2	426.4	426.0	423.0	436.3	433.6	432.4	423.0	436.3	433.6	432.4				
Jefferson Barracks	169.3	424.2	425.0	424.5	424.1	420.7	435.2	432.0	430.9	420.7	435.2	432.0	430.9				
Waters Point	158.5	415.4	419.0	418.5	418.1	412.2	429.6	426.8	425.3	412.2	429.6	426.8	425.3				
Selma	146.0	409.5	412.4	411.8	411.2	405.9	423.5	419.5	418.2	405.9	423.5	419.5	418.2				
Brickeye	136.0	405.2	409.2	408.5	407.6	401.5	417.3	413.3	411.8	401.5	417.3	413.3	411.8				
Little Rock Ldg.	125.5	399.5	400.9	399.3	397.6	393.2	410.6	405.9	404.4	393.2	410.6	405.9	404.4				
East Kaskaskia	116.2	395.6	395.3	395.0	391.8	406.6	403.1	402.3	391.9	406.6	403.1	402.3	391.9				
Chester	109.5	391.1	390.8	390.4	386.9	402.5	398.3	398.0	387.1	402.4	398.3	398.2	397.9				
Blahop Ldg.	100.8	385.4	388.0	387.2	386.8	383.3	398.7	393.4	392.5	383.5	398.7	393.4	392.5				
Red Rock Ldg.	94.1	381.7	384.6	384.5	384.3	381.2	395.8	390.8	389.9	381.5	395.8	390.8	389.9				
Cumberland Rock	87.0	377.2	379.5	379.1	378.8	376.9	390.3	384.8	384.4	377.4	390.3	384.8	384.1				
Grand Tower	81.0	373.1	376.2	376.0	375.9	374.6	385.3	382.0	381.5	375.3	385.0	381.7	381.2				
Crawford Ldg.	72.9	368.3	369.7	369.4	369.2	366.0	378.1	374.4	373.6	367.1	377.6	373.9	373.2				
Moccasin Springs	66.3	364.6	365.3	365.1	365.0	361.8	372.8	370.0	369.5	362.8	372.2	369.4	368.9				
Devile Island	57.3	360.3	362.2	361.9	361.7	361.2	369.3	366.2	366.0	362.5	368.6	365.6	365.4				
Cape Girardeau	52.1	356.4	359.8	359.4	359.2	358.5	361.6	360.6	360.5	358.7	360.5	359.6	359.4				
Grays Point*	46.3	350.4	353.7	353.7	353.7	353.7	353.7	353.7	353.7	353.7	353.7	353.7	353.7				
Thebes	43.7										349.2	349.2	349.2				
Counterfeit Rock	42.3										346.7	346.7	346.7				
Commerce*	39.3										344.4	344.4	344.4				

* Water surface at Grays Point was held to a rating curve developed from model test results in NRM Report 31-5, Flow Line Study, Mississippi and Illinois Rivers, June 1977.



Photo 1. Series I - Folded screen wire simulating overbank roughness fully developed in its natural state on all areas between river and its bluff line or levee



Photo 2. Series II - Folded screen wire simulating overbank roughness fully developed in its natural state on areas where vegetation existed in 1973



Photo 3. Series III - Folded screen wire simulating overbank roughness where vegetation existed in 1973 installed to density required to reproduce 1973 flood stages

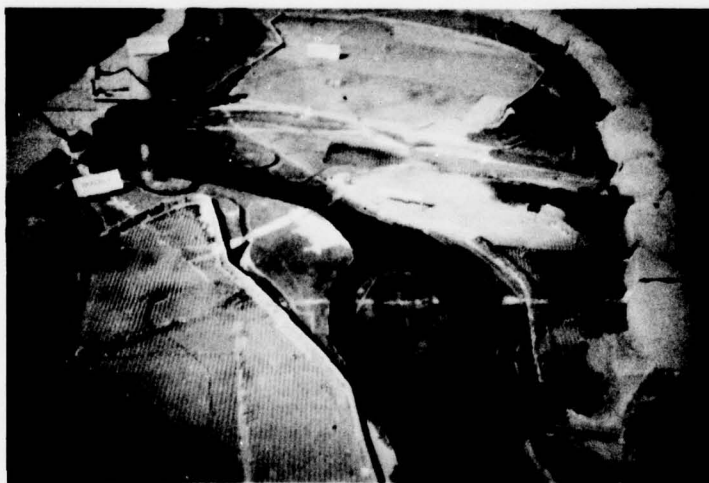


Photo 4. Series IV - Folded screen wire simulating overbank roughness removed from all areas between the river and its bluff line or levee

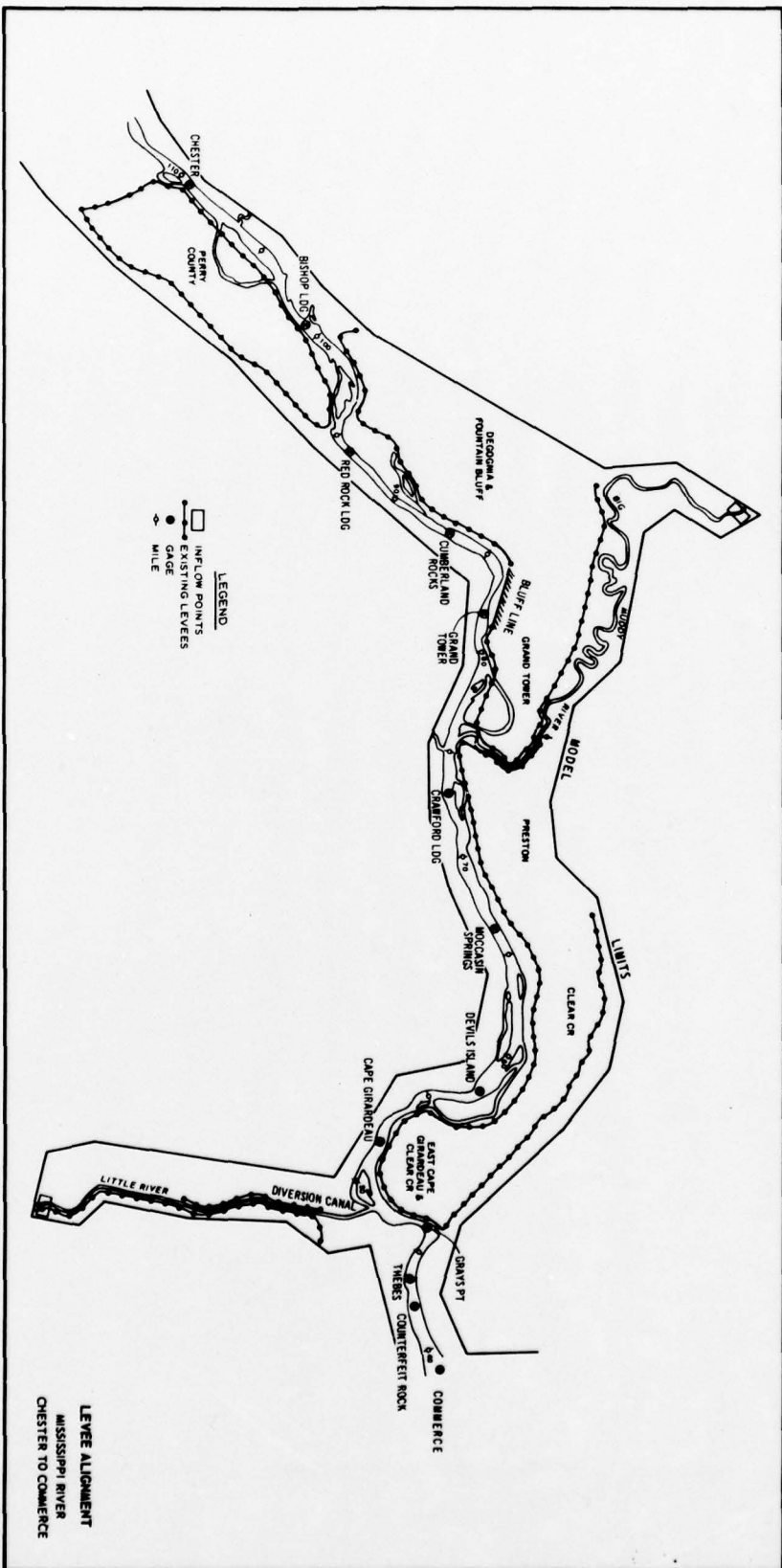
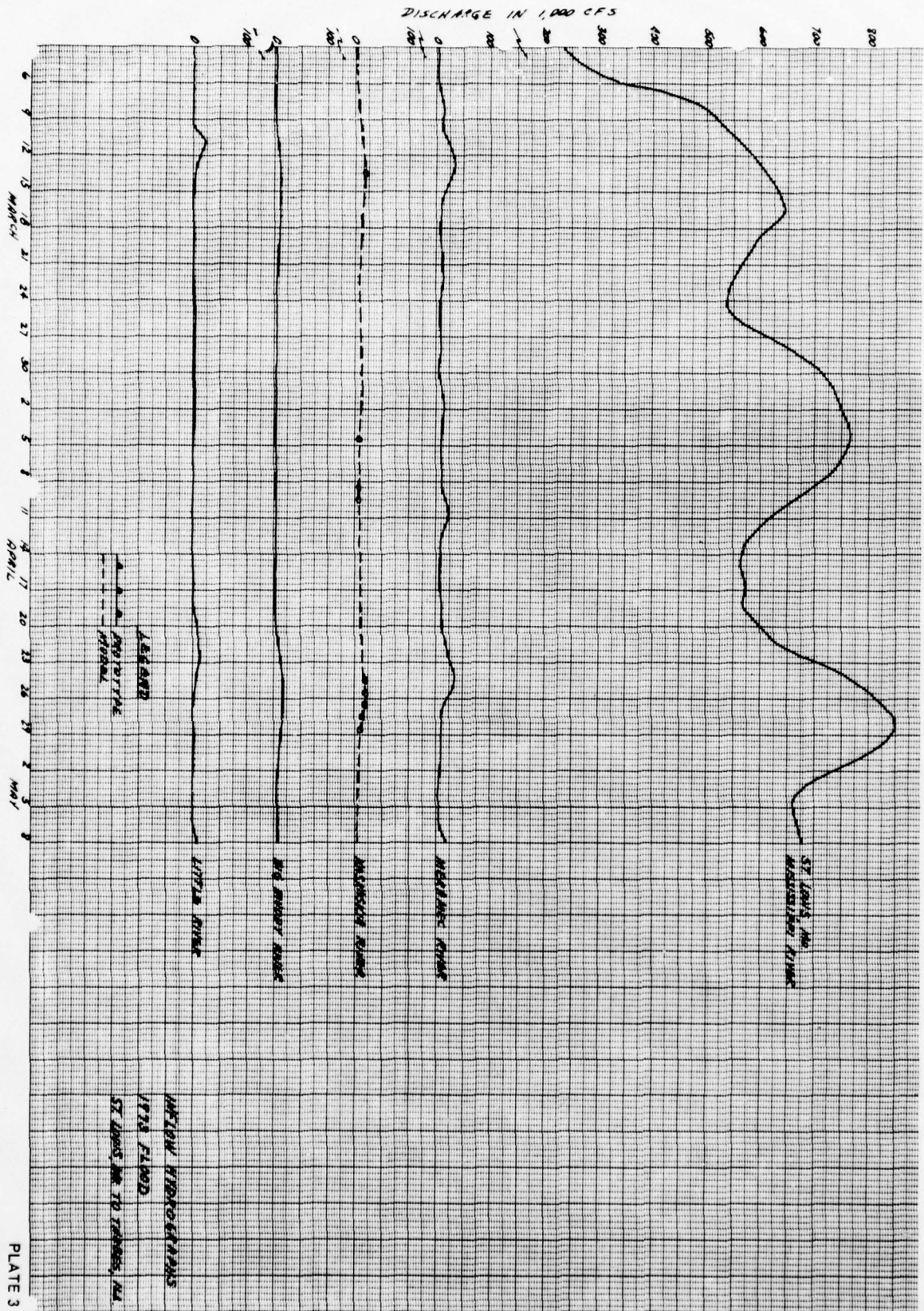
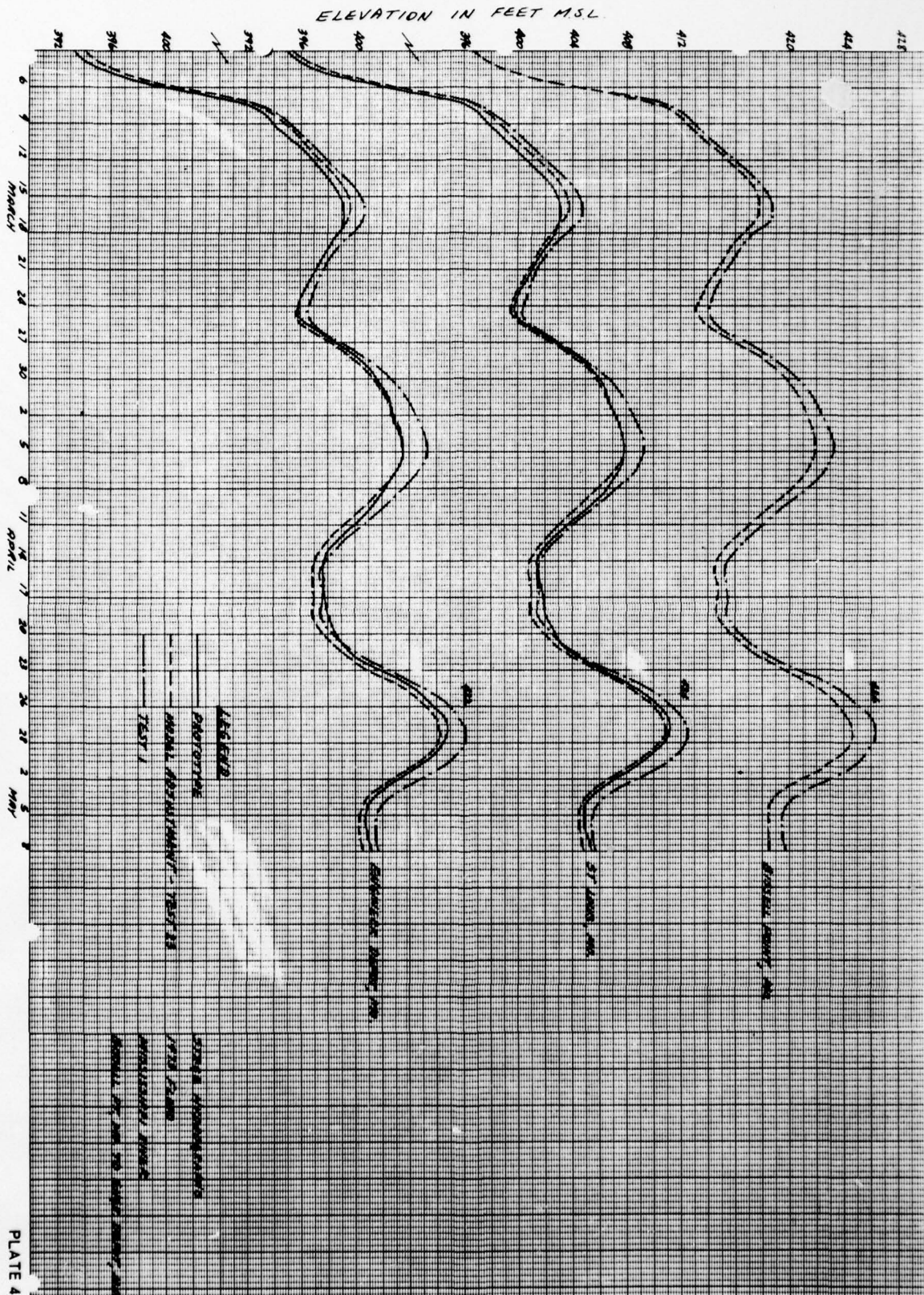
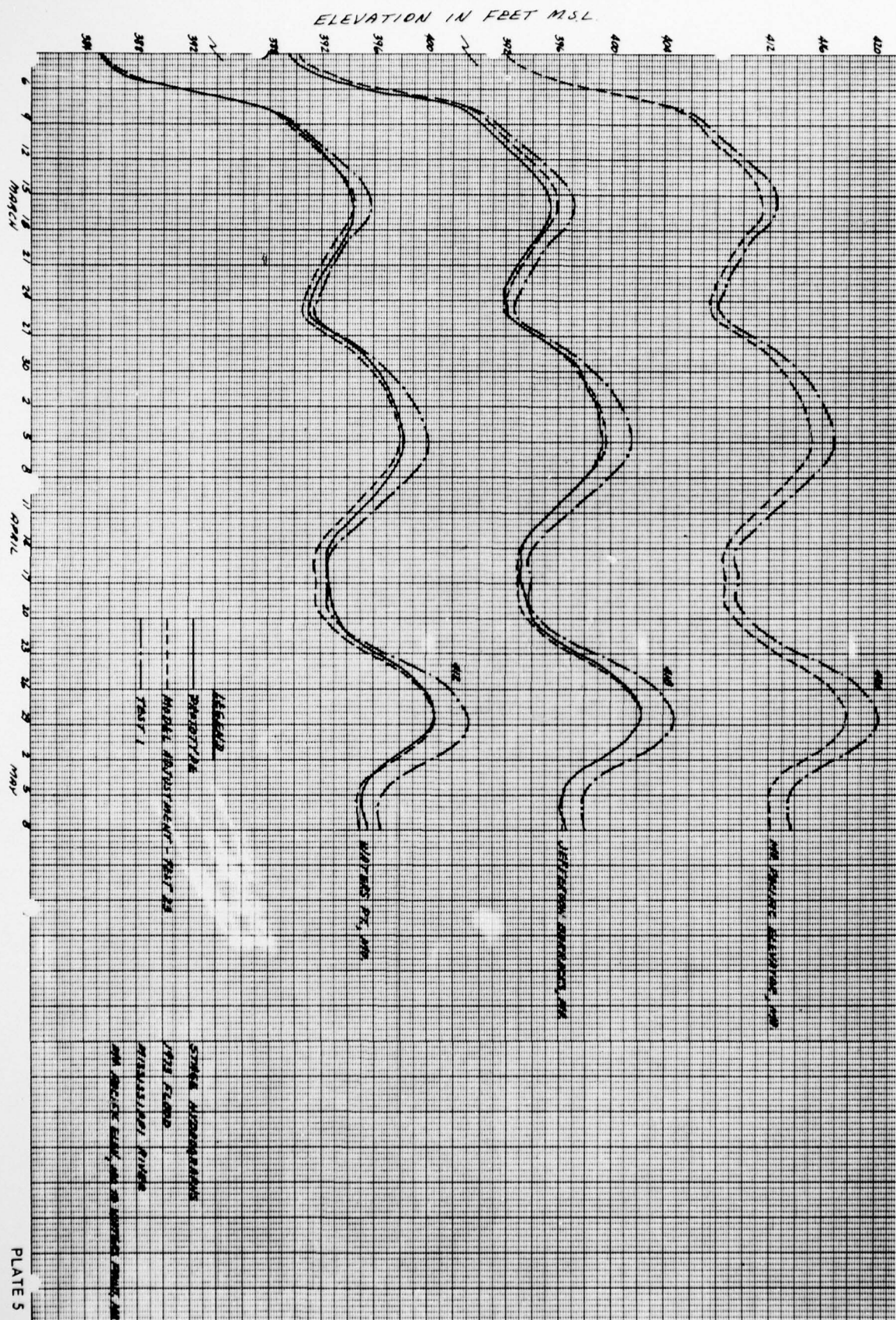


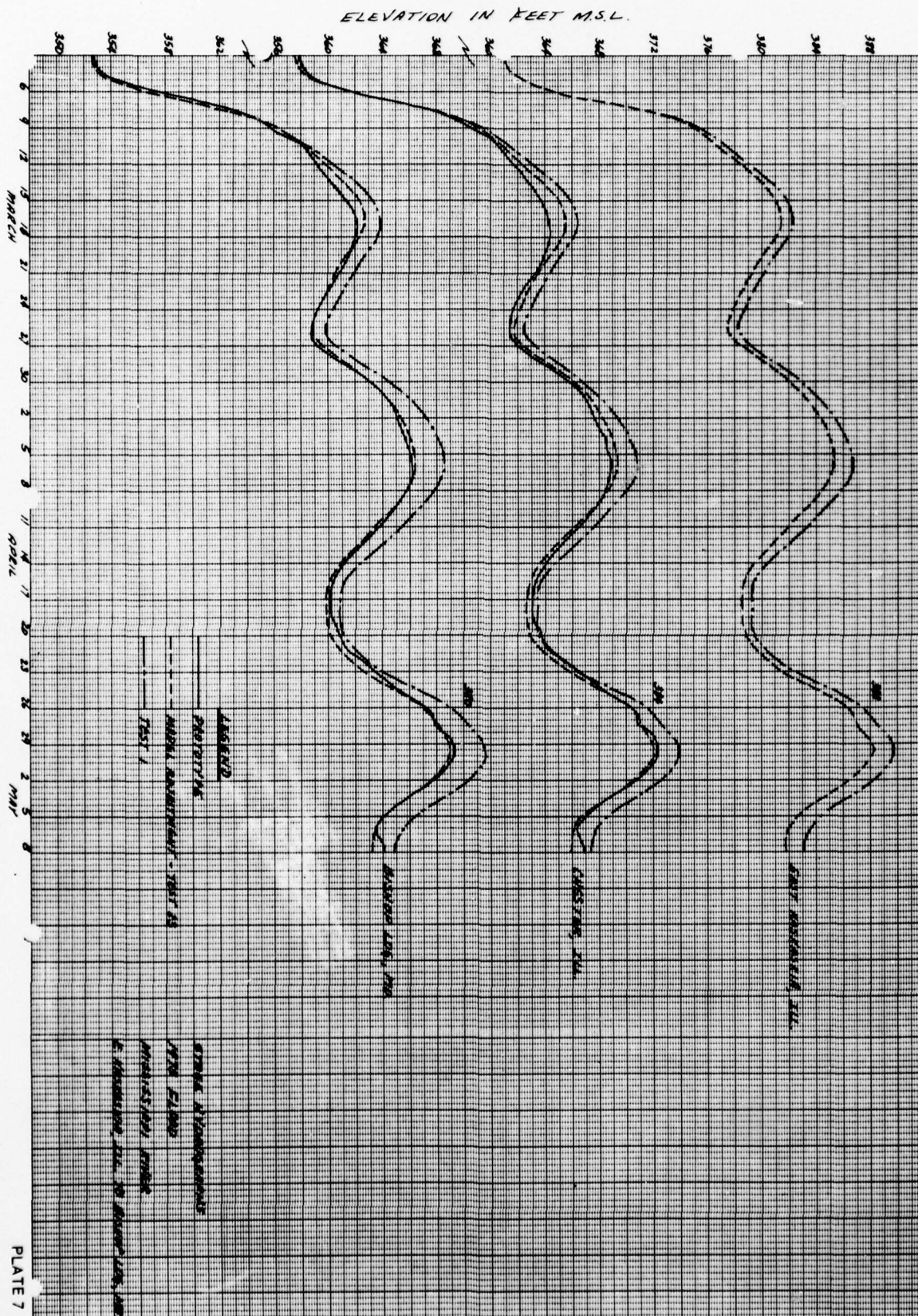
PLATE 2

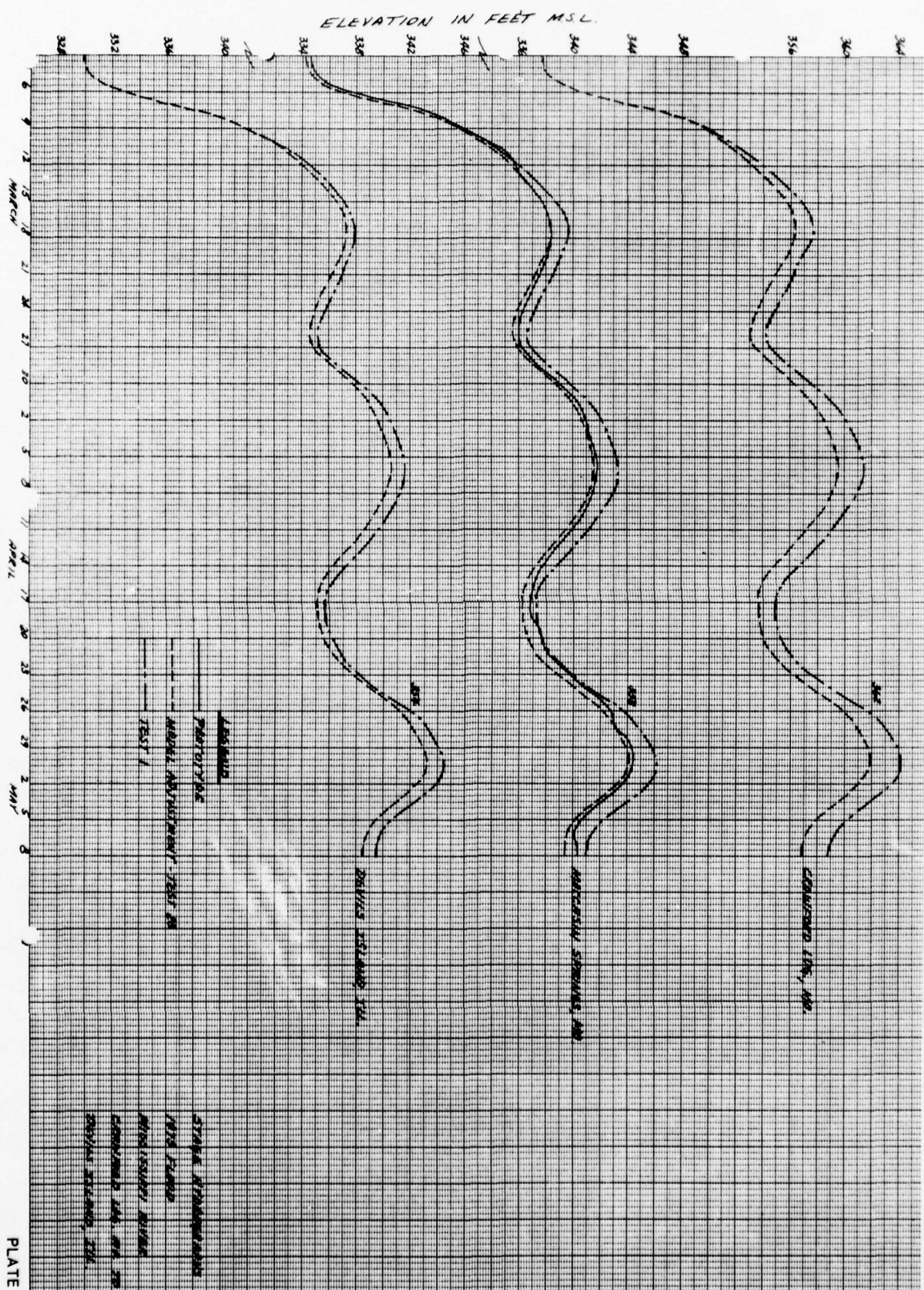
LEVEE ALIGNMENT
MISSISSIPPI RIVER
CHESTER TO COMMERCE

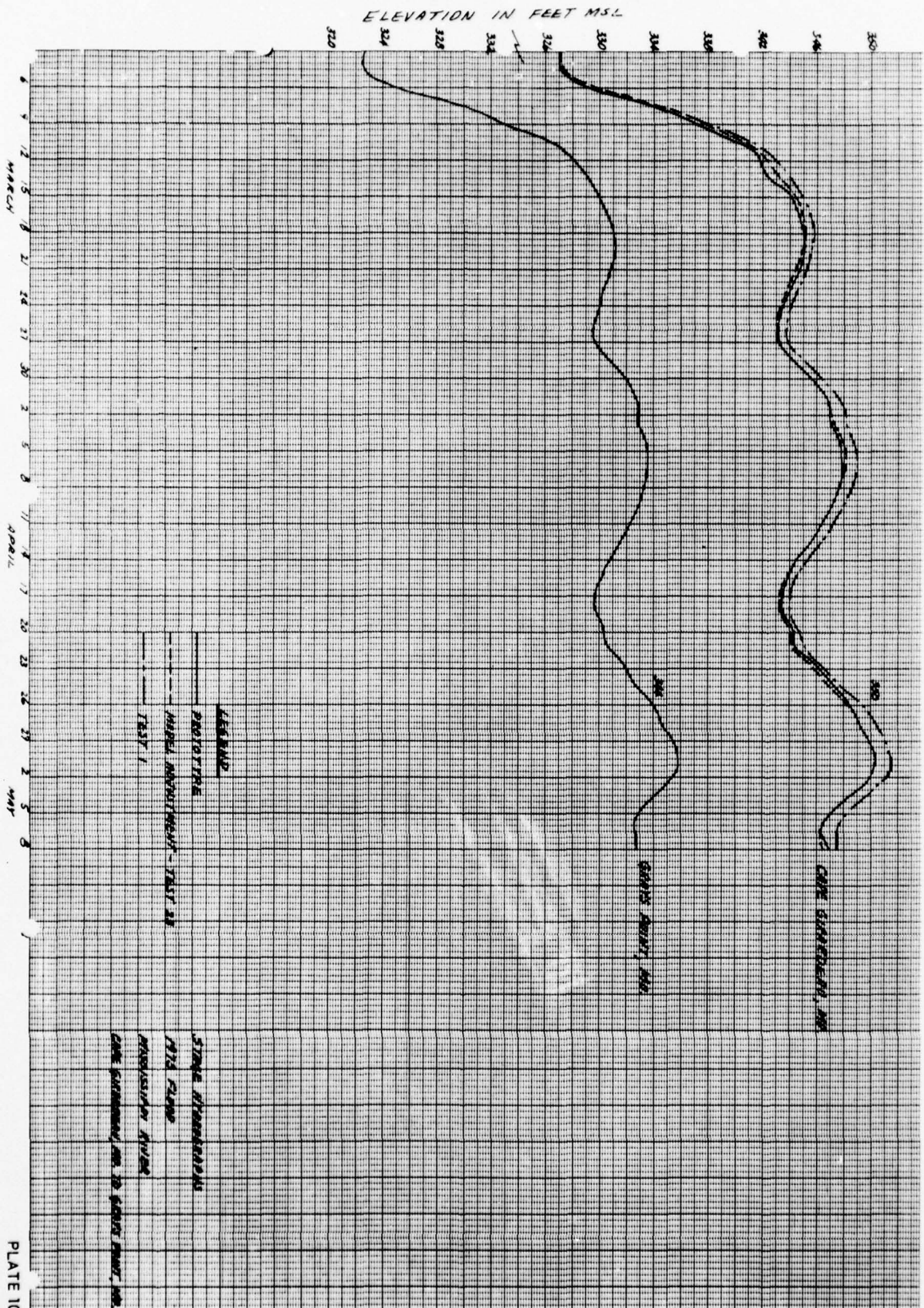


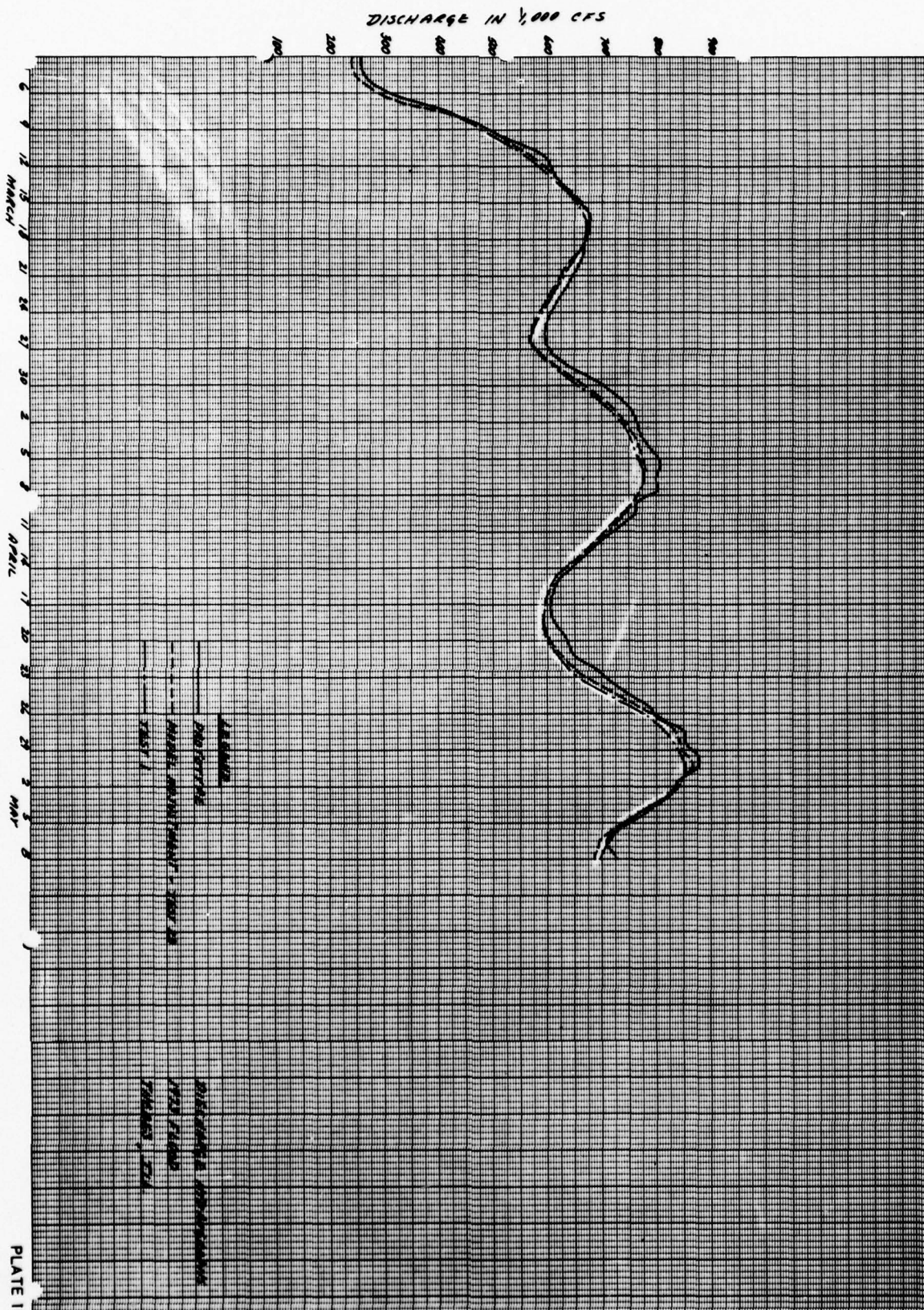


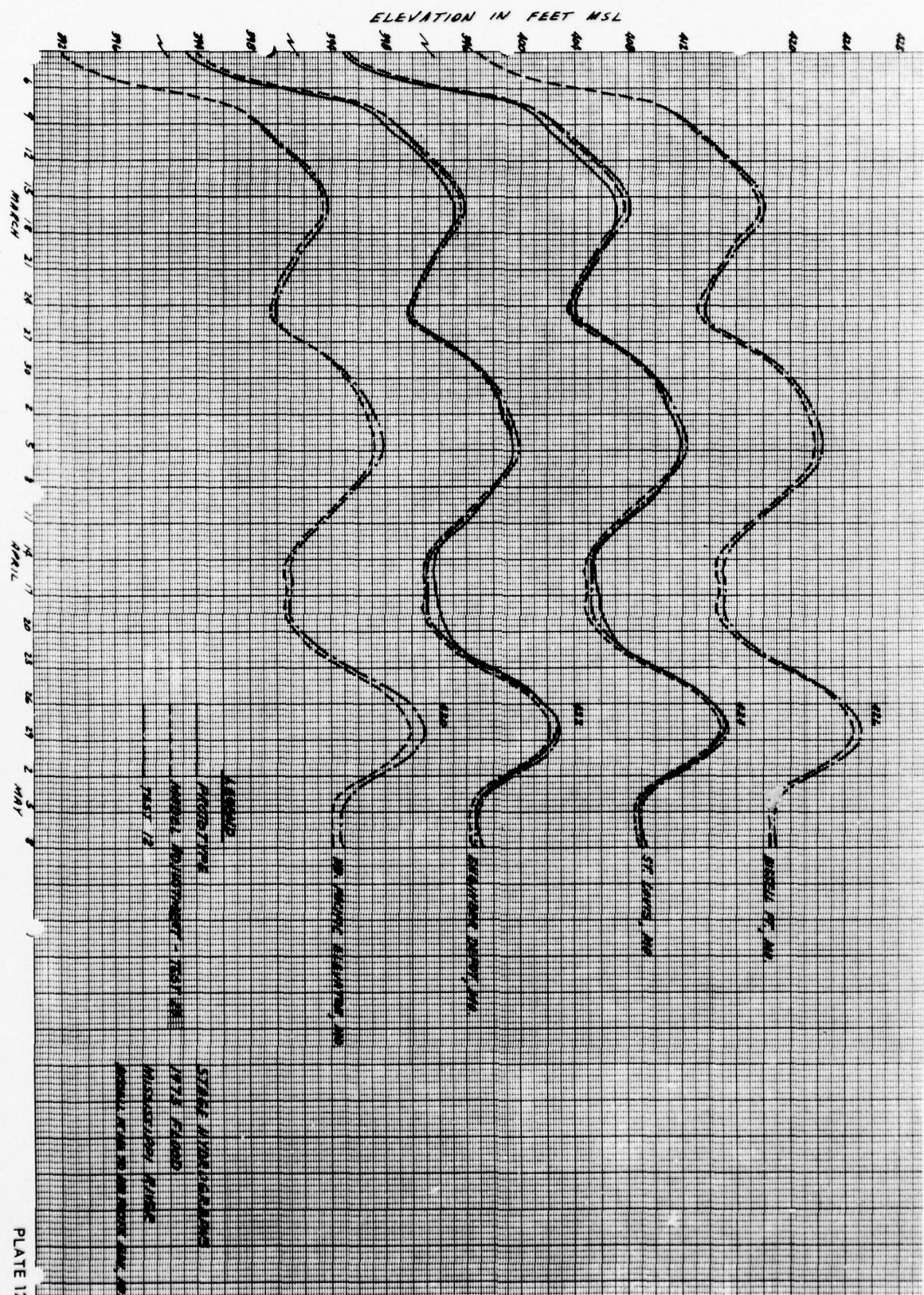


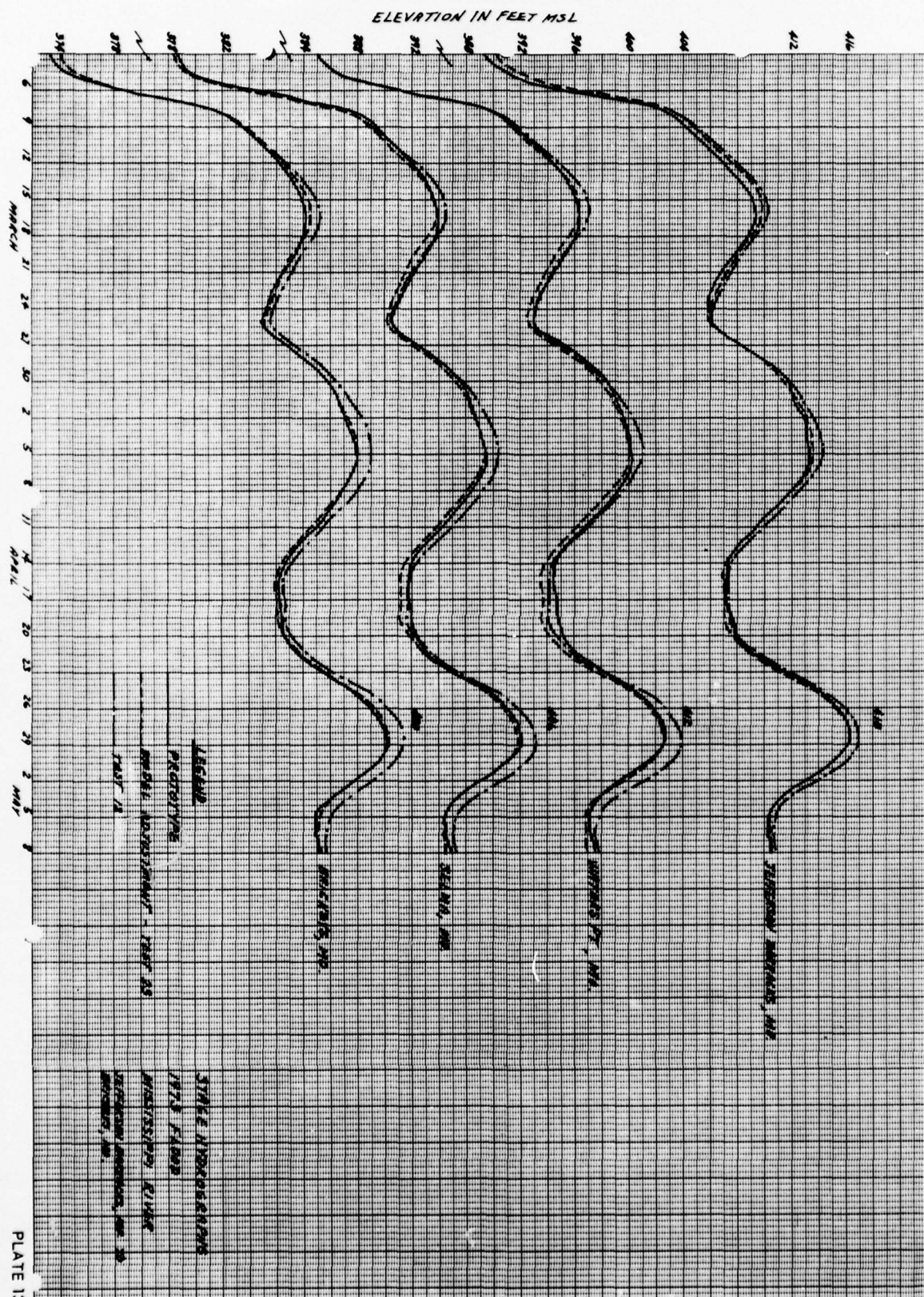


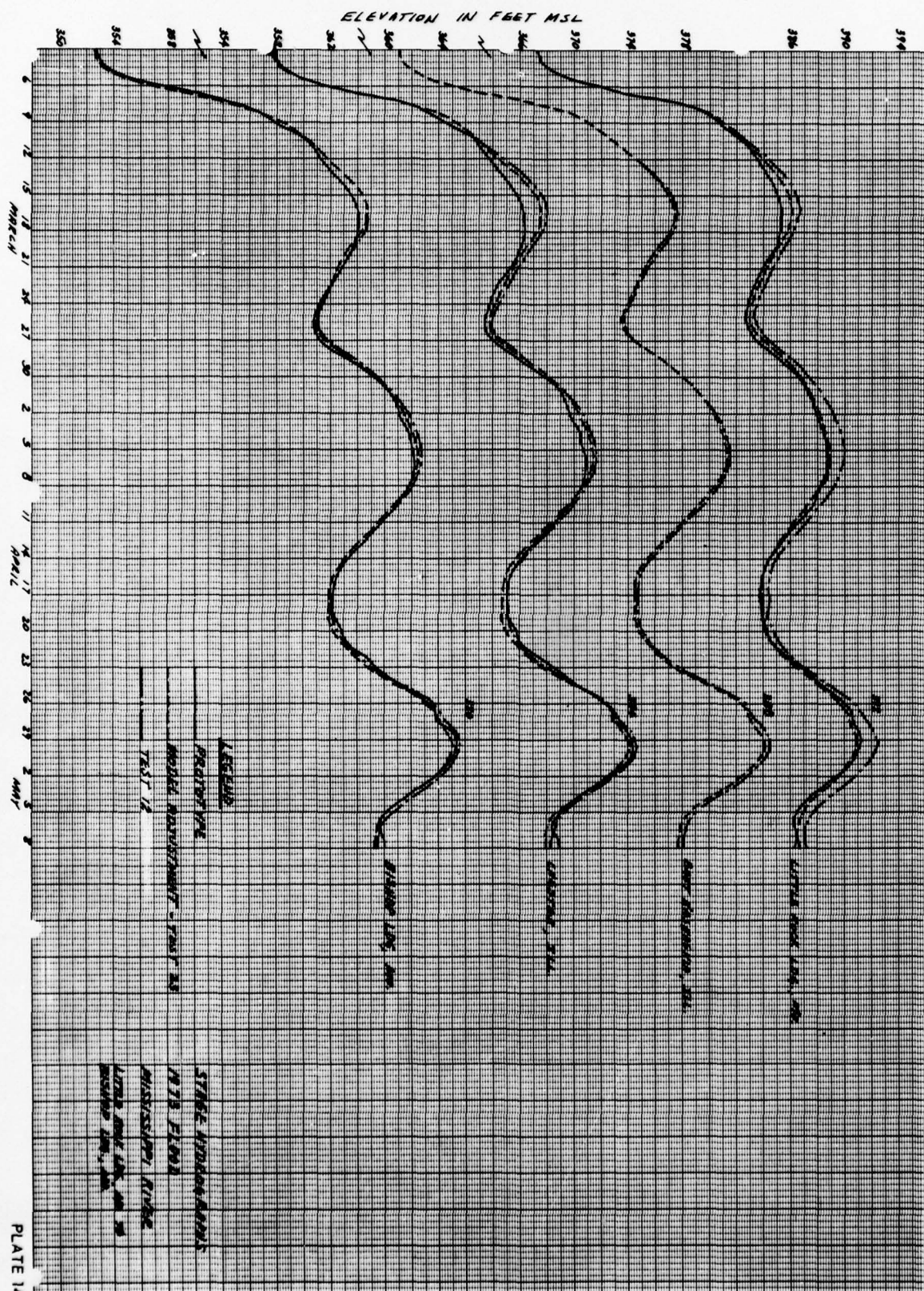


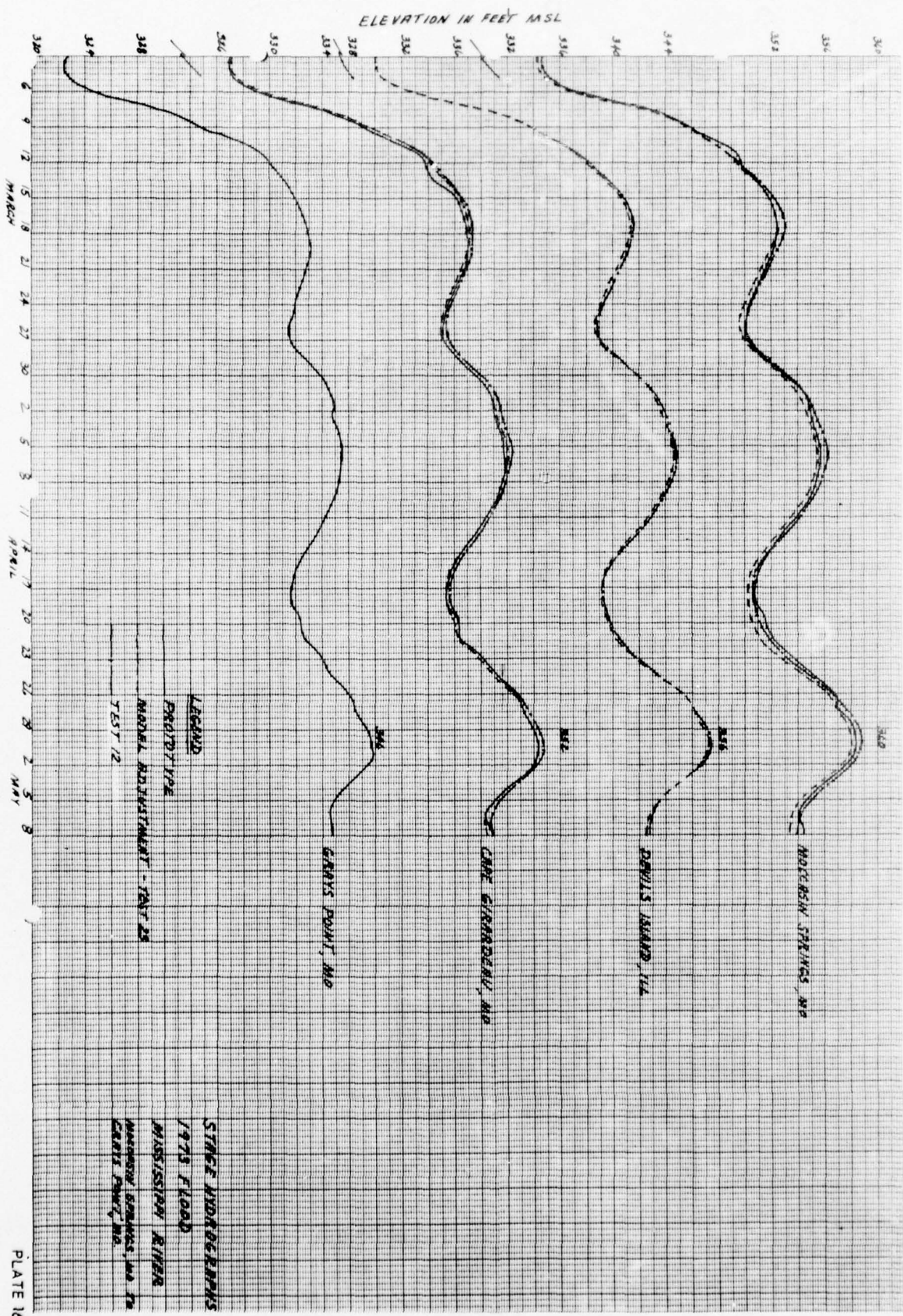


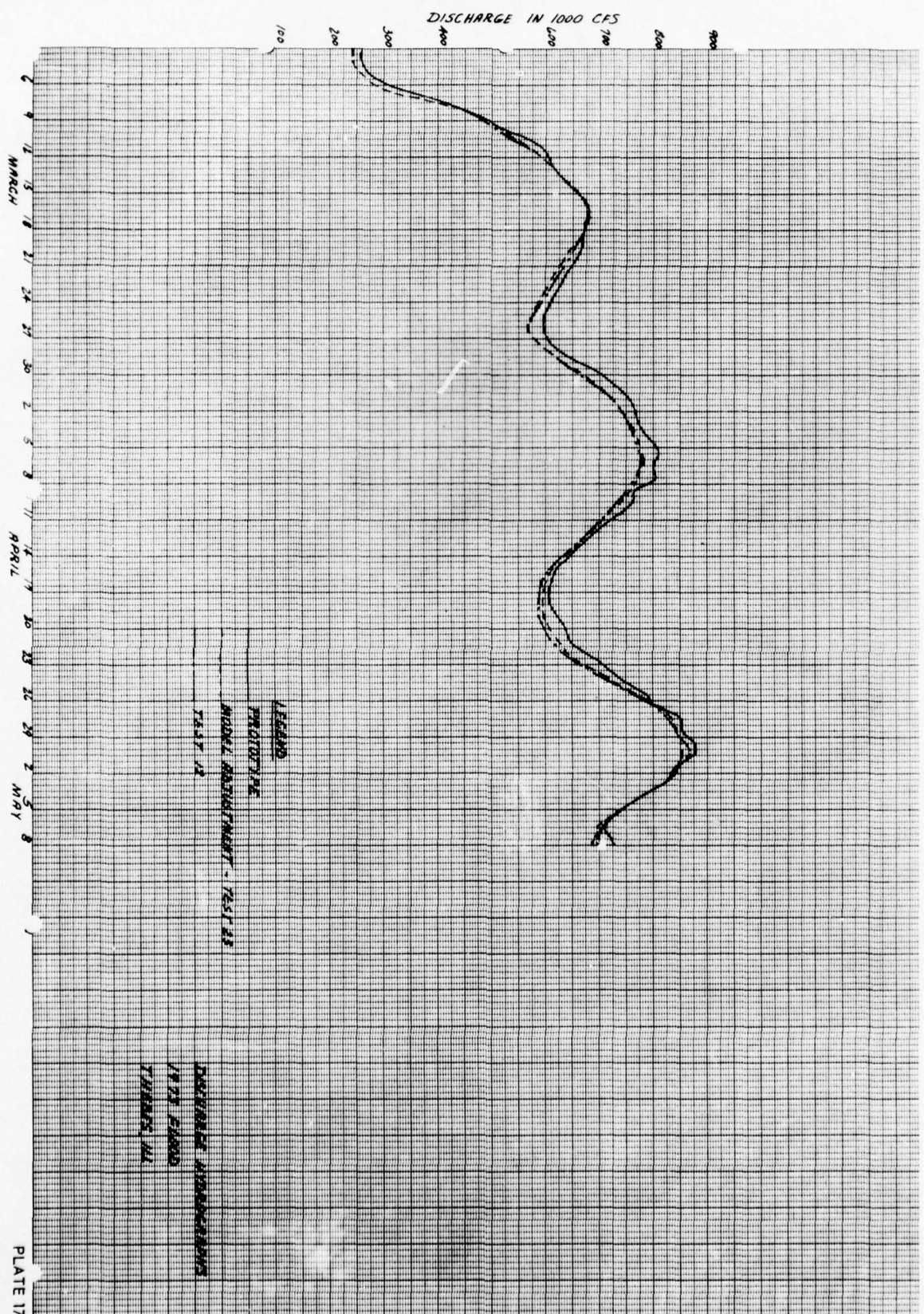


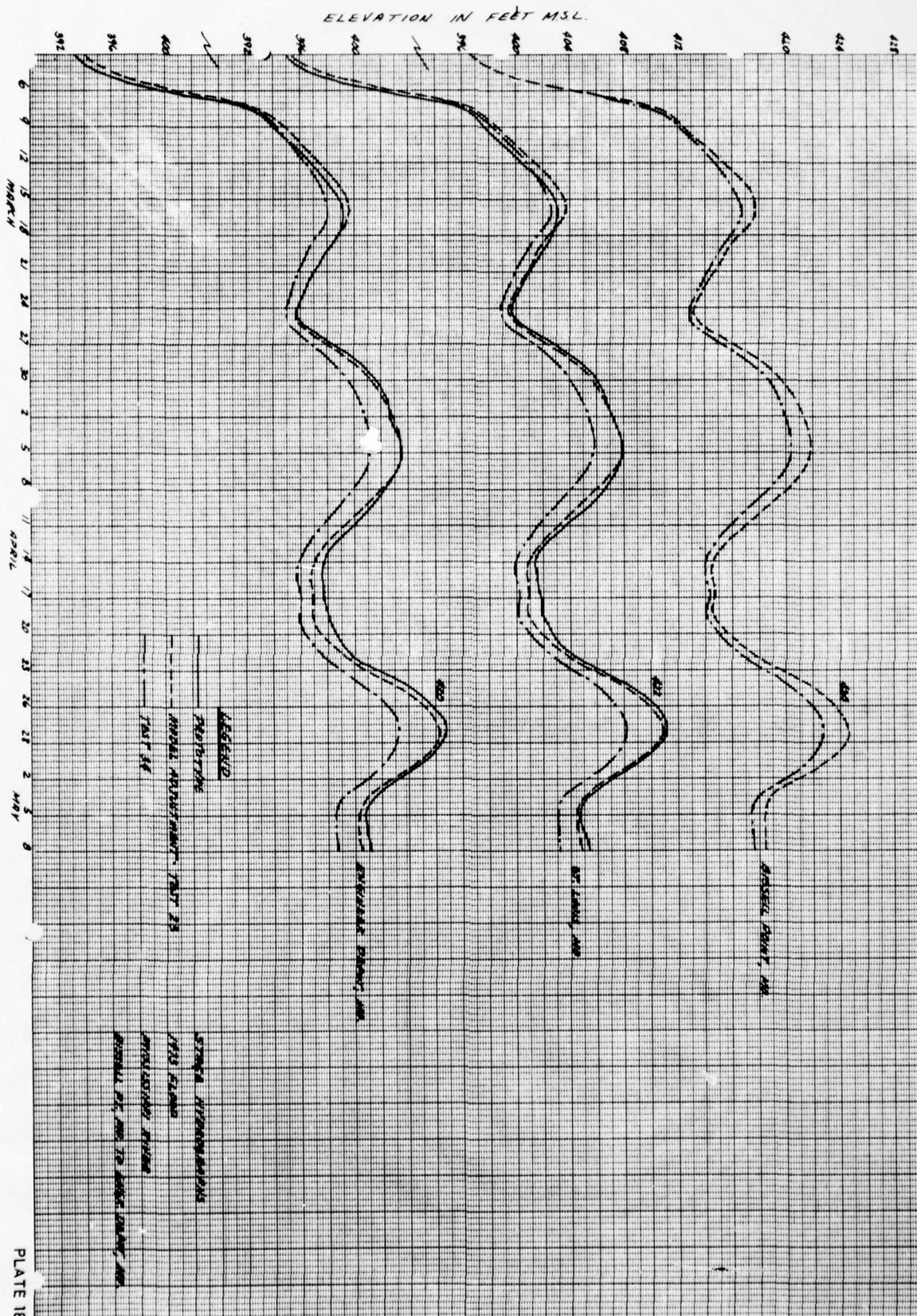


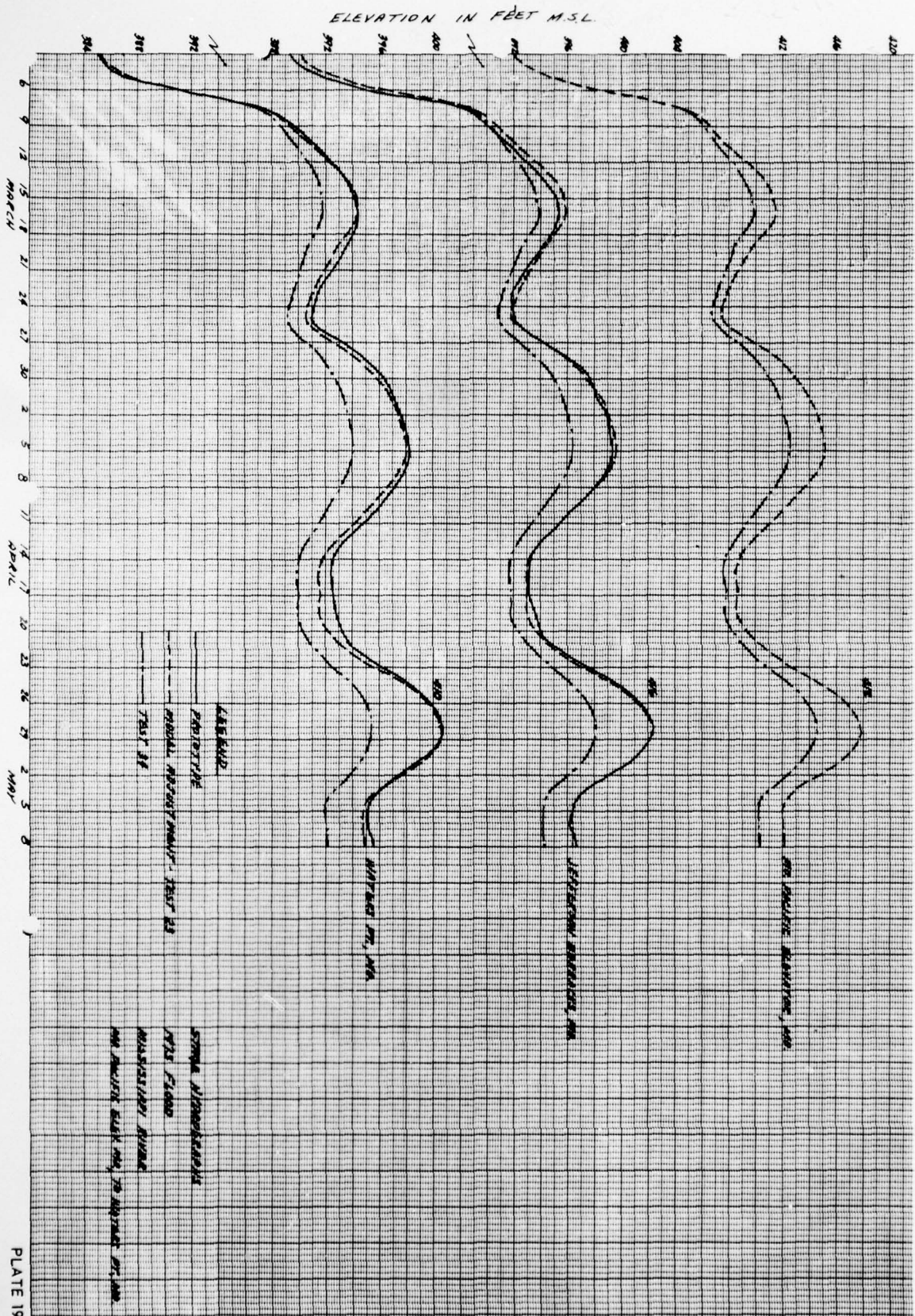


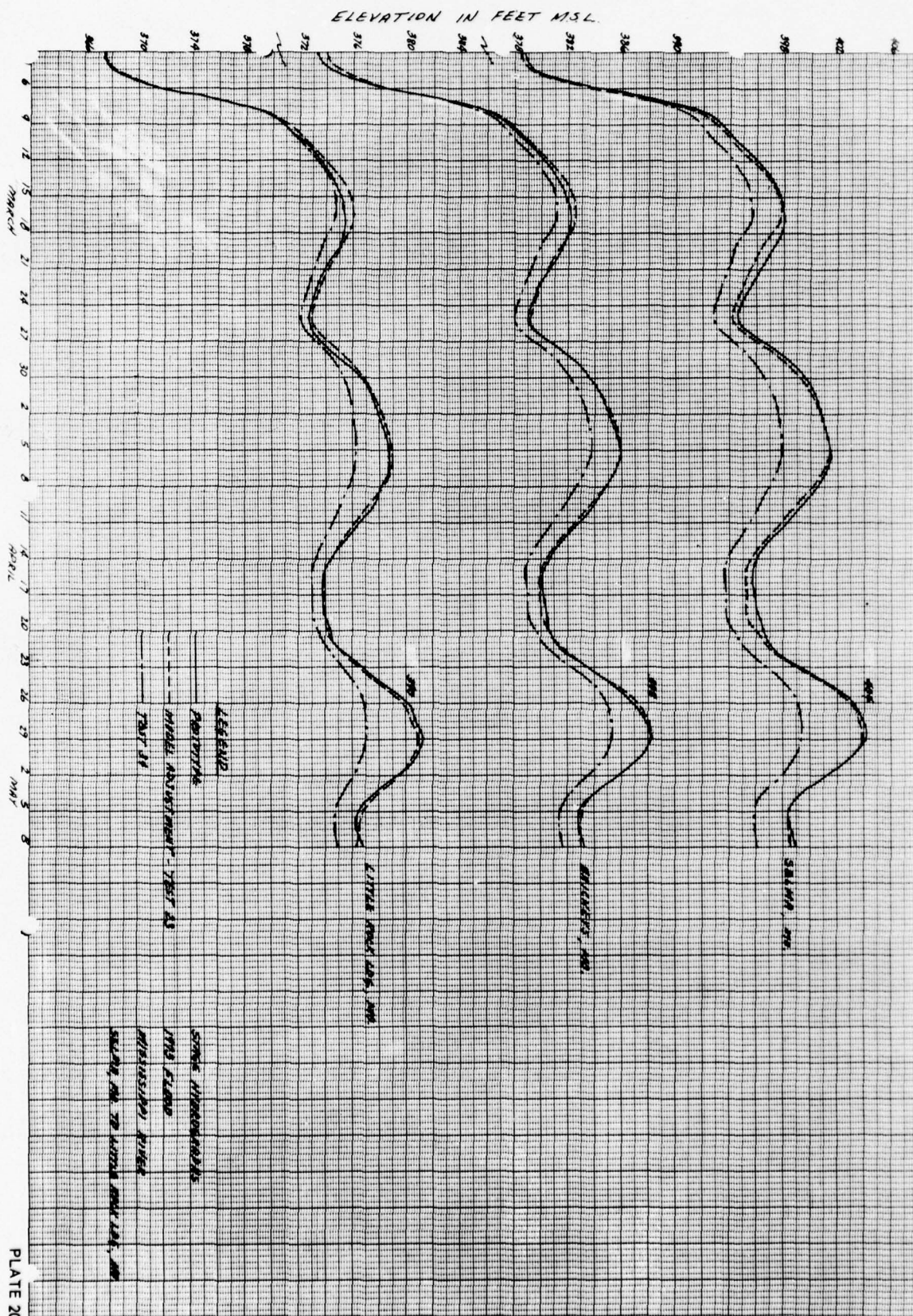


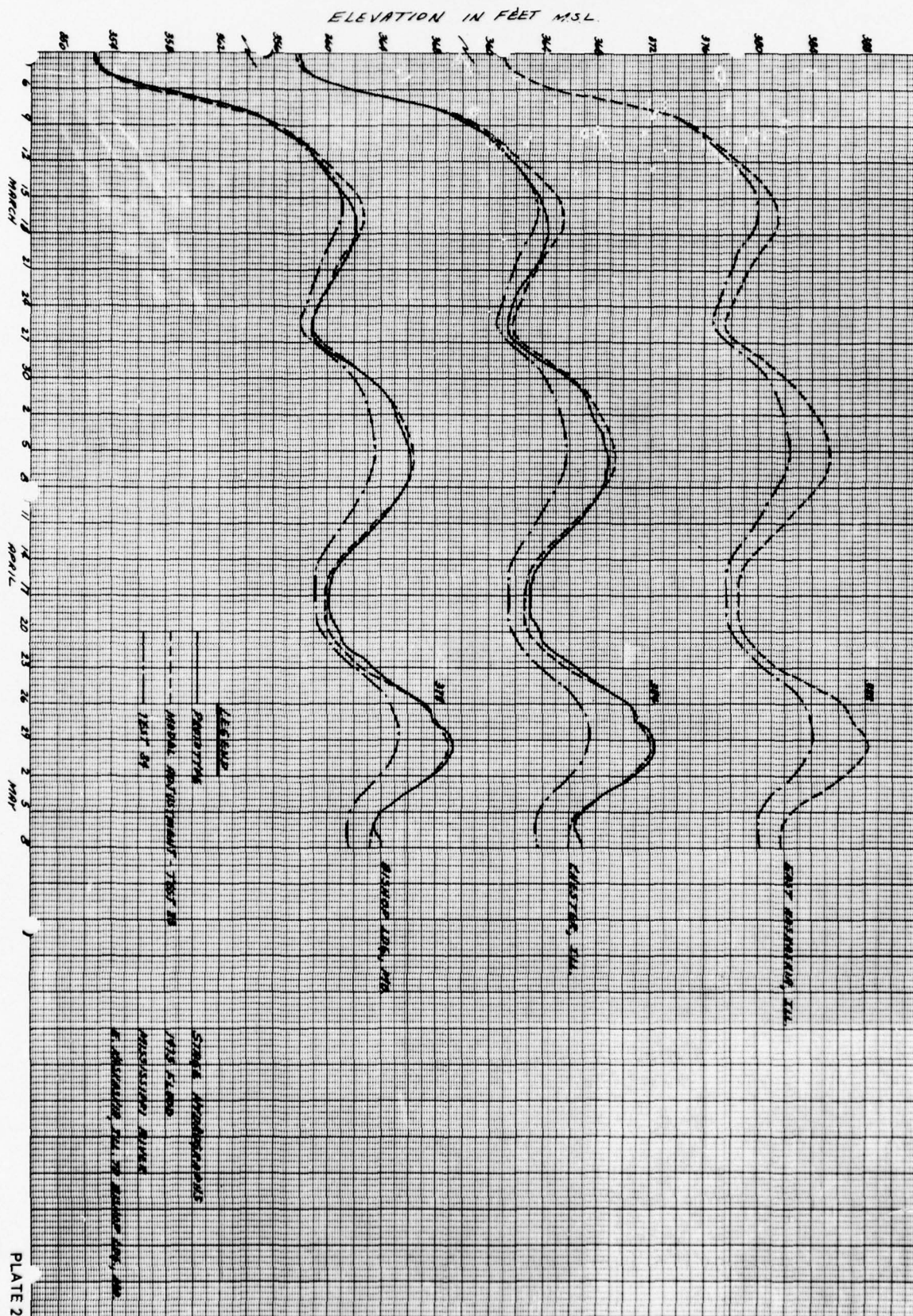


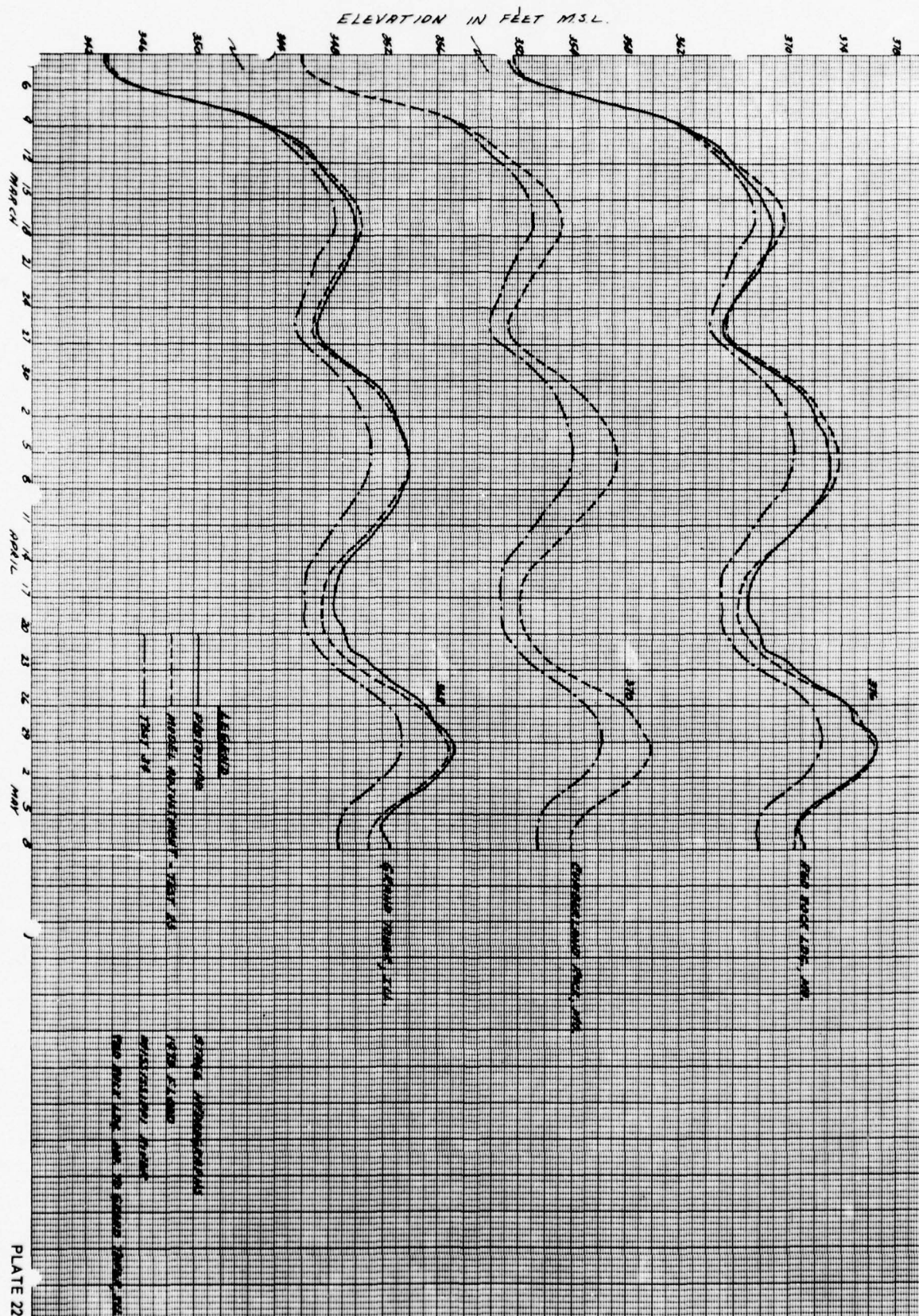


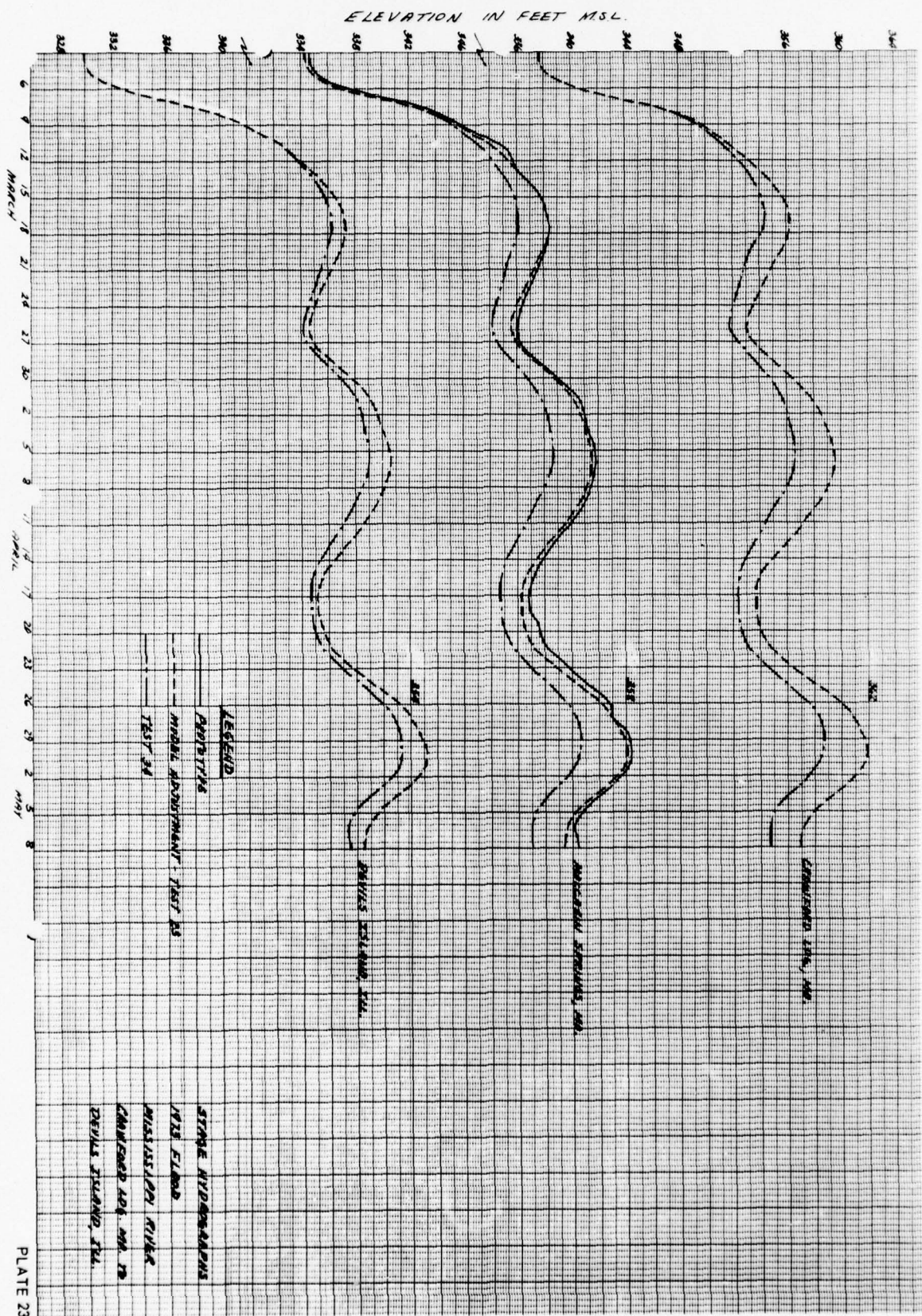


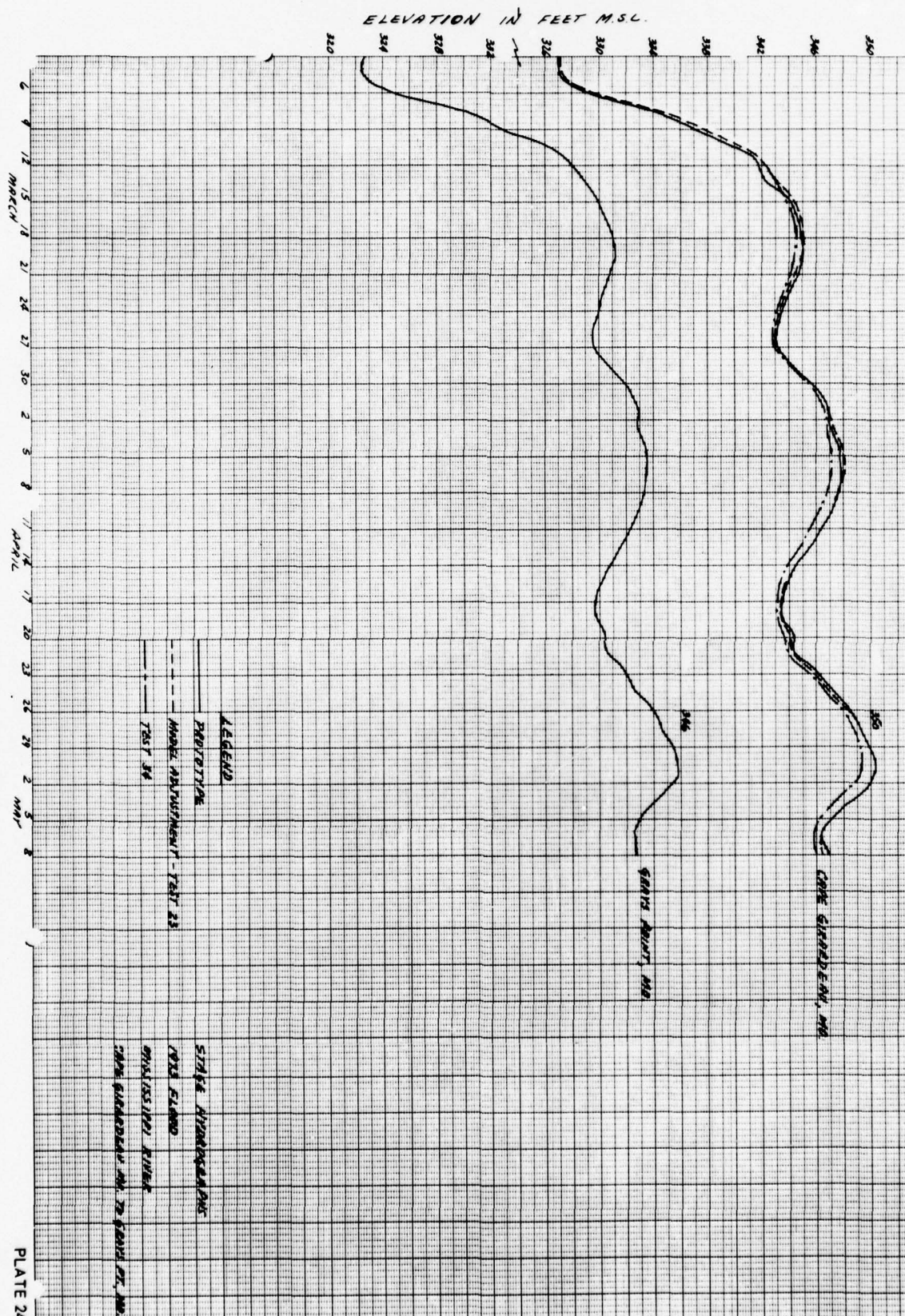


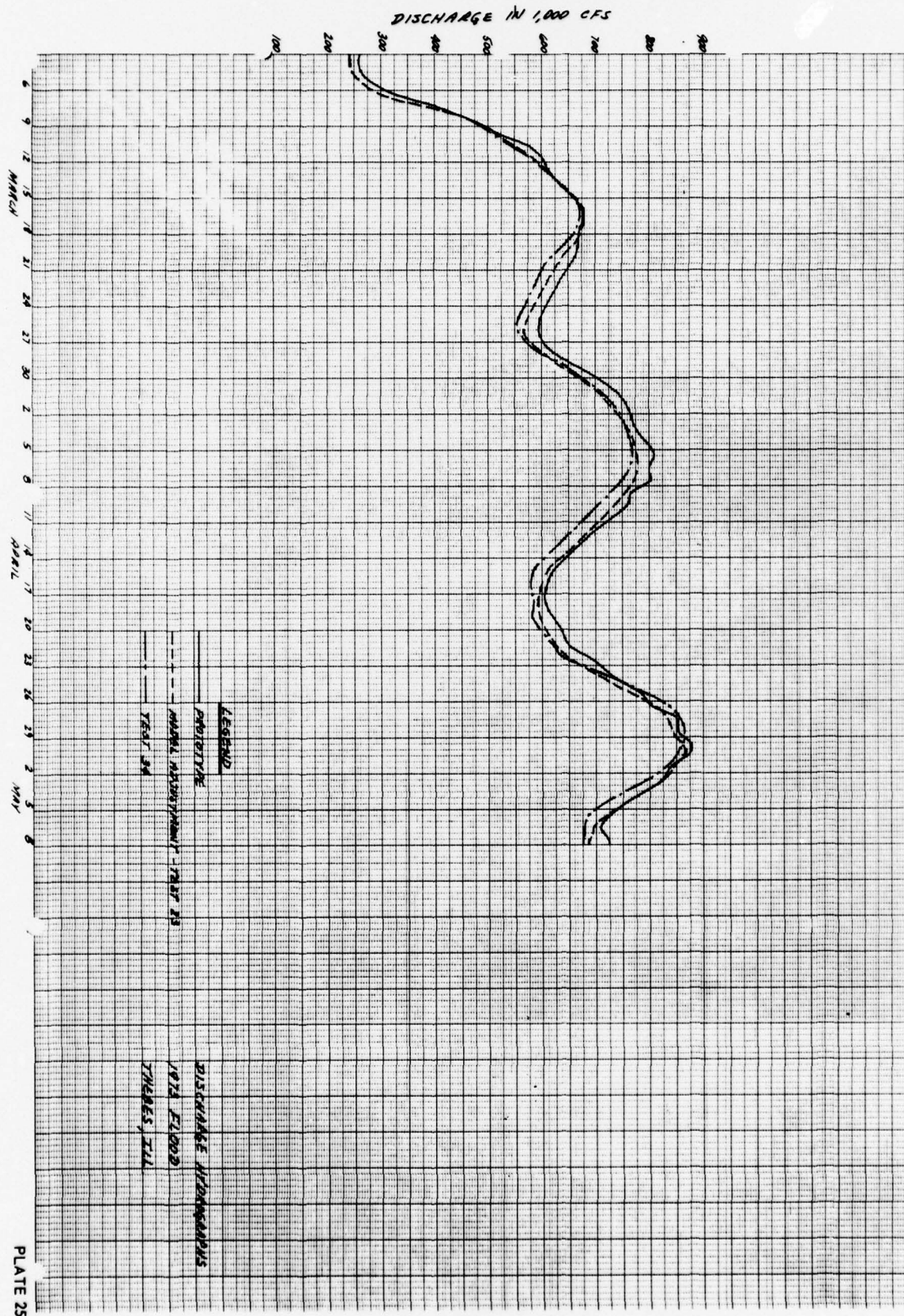


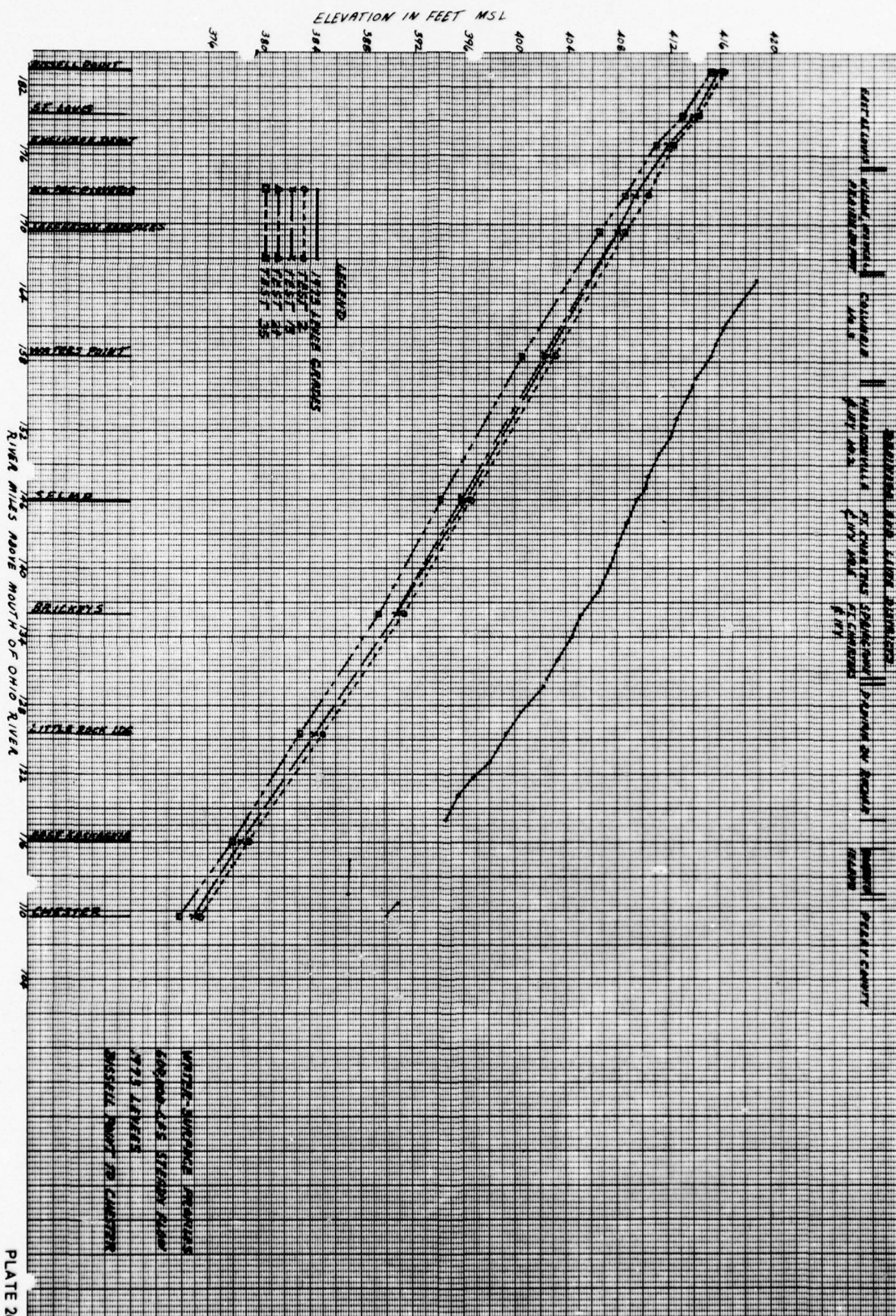


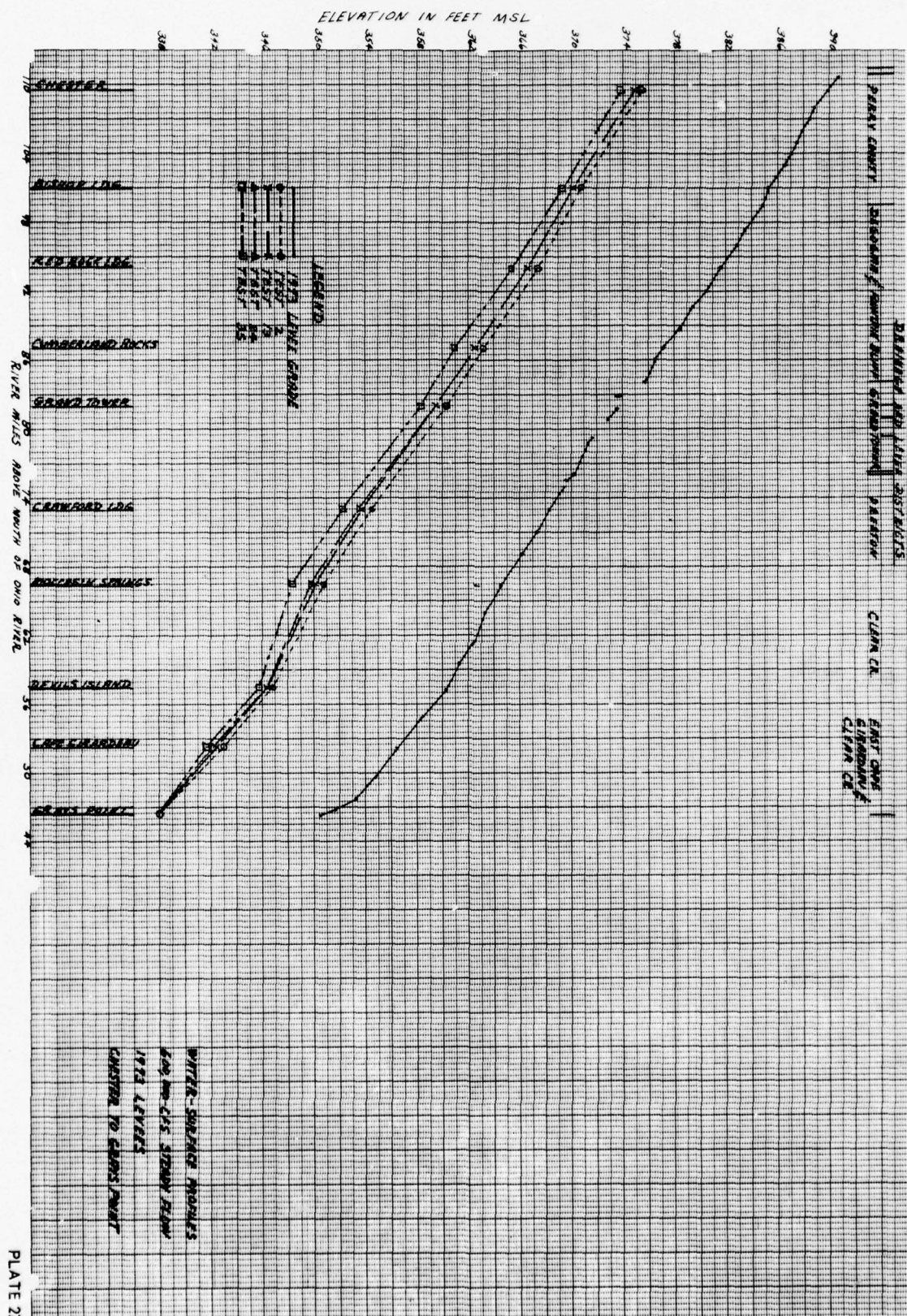


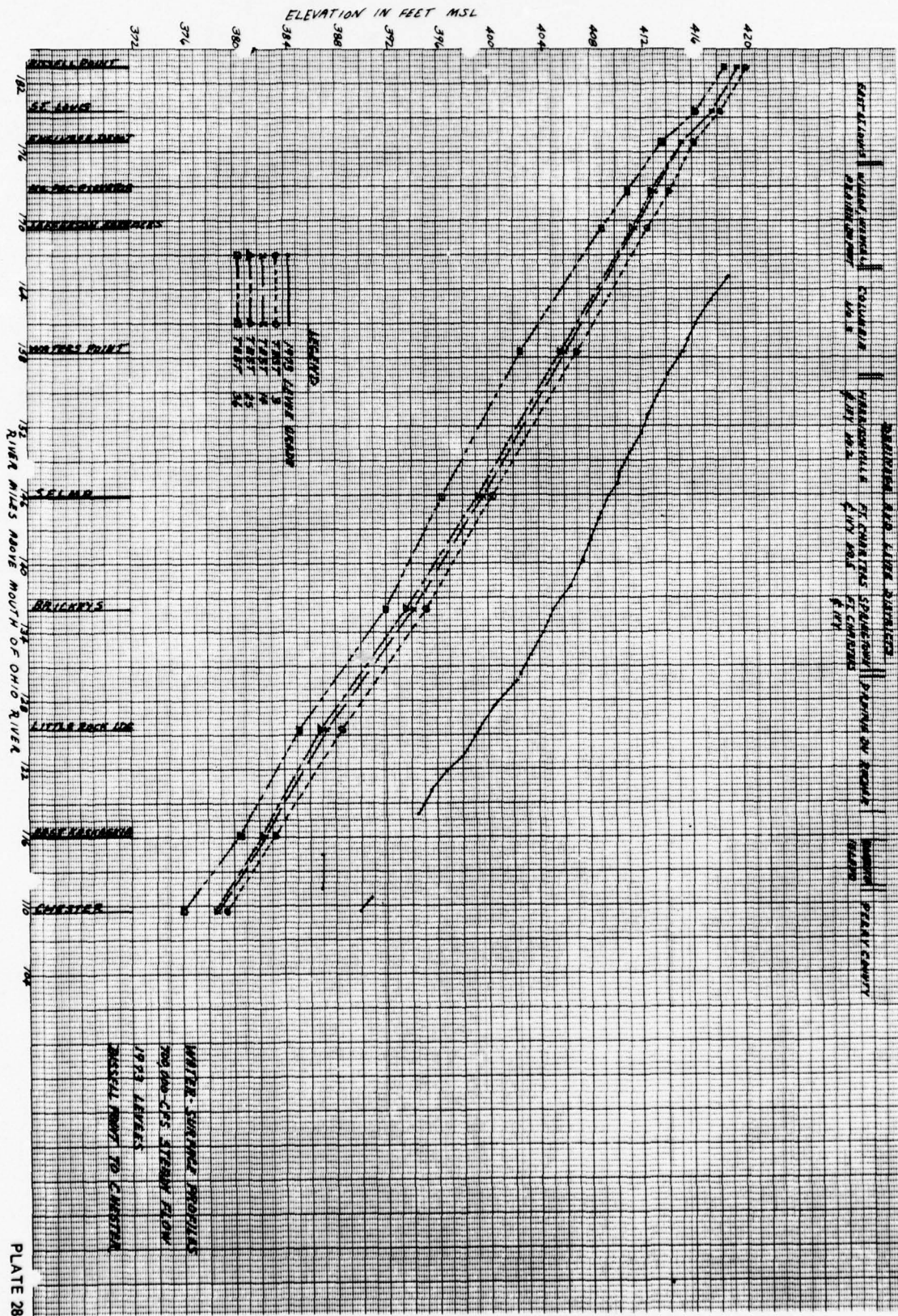


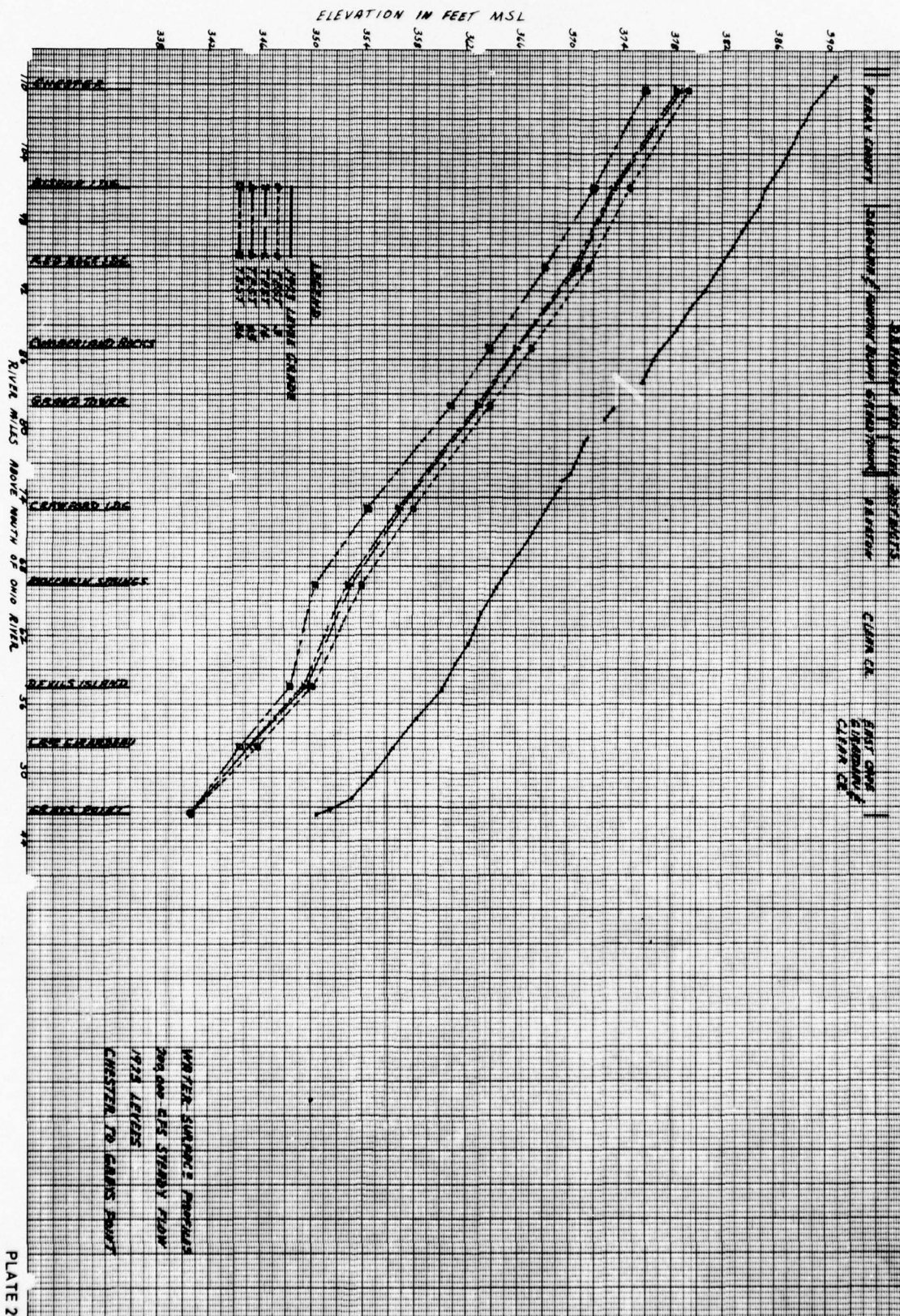


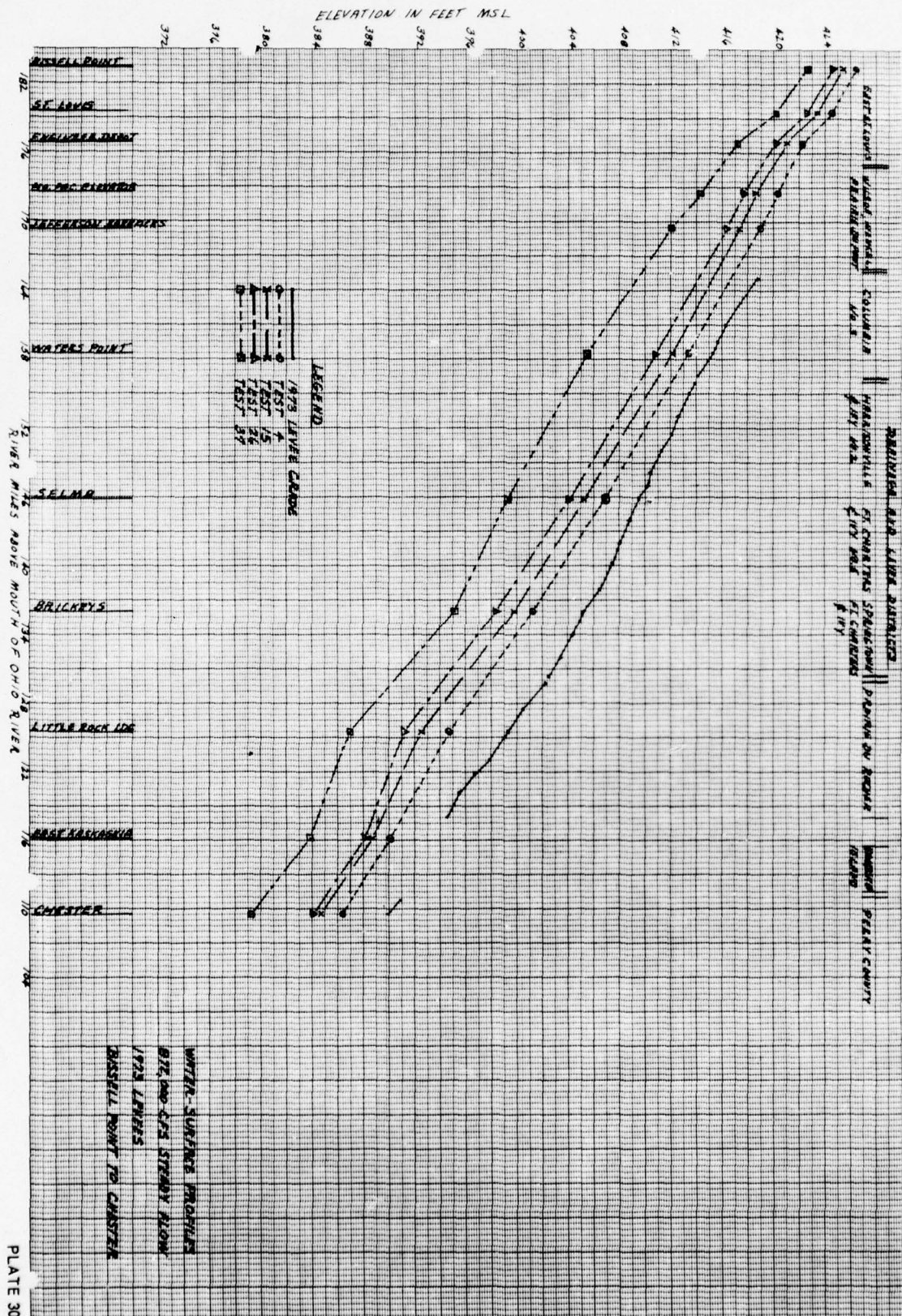


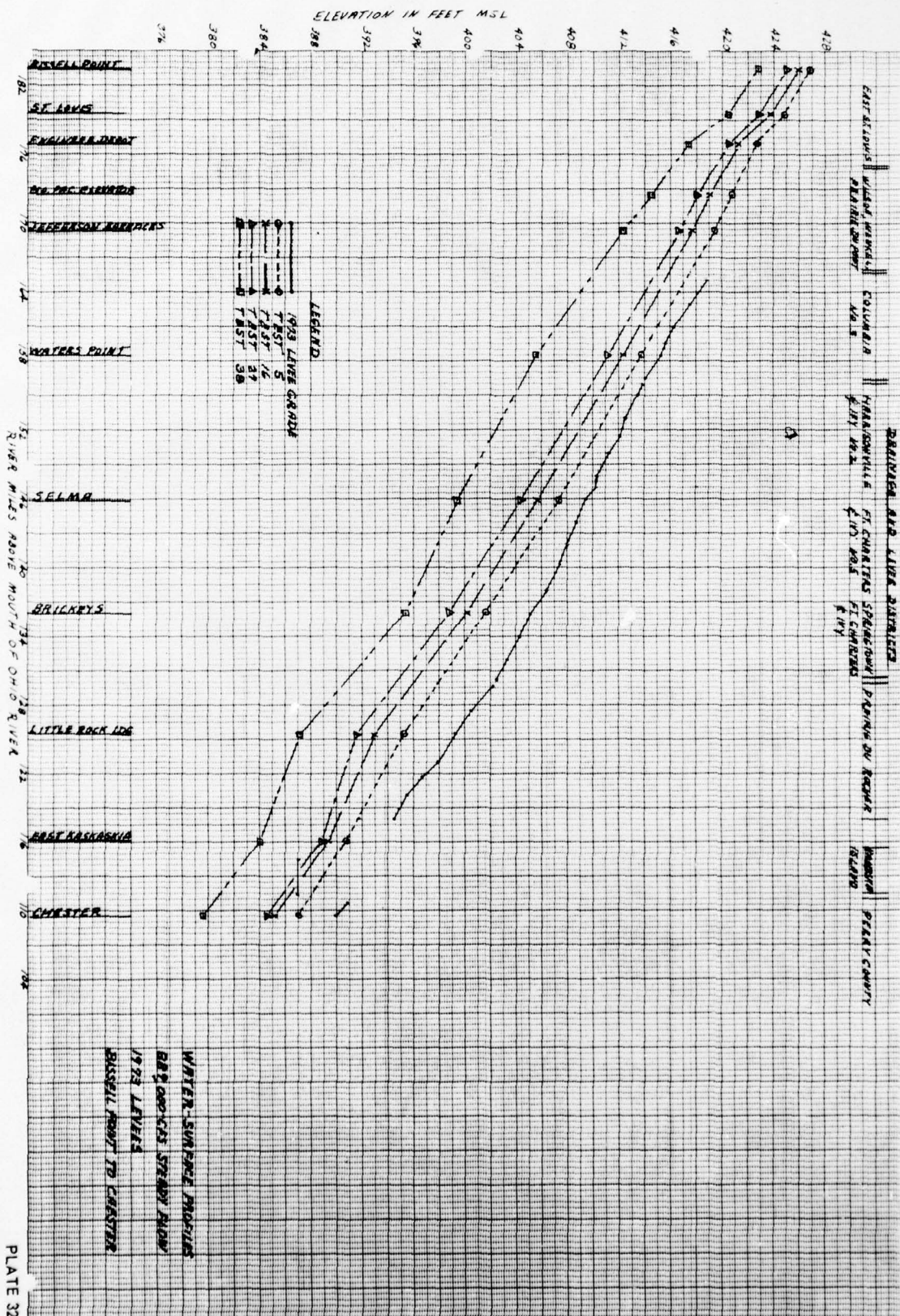


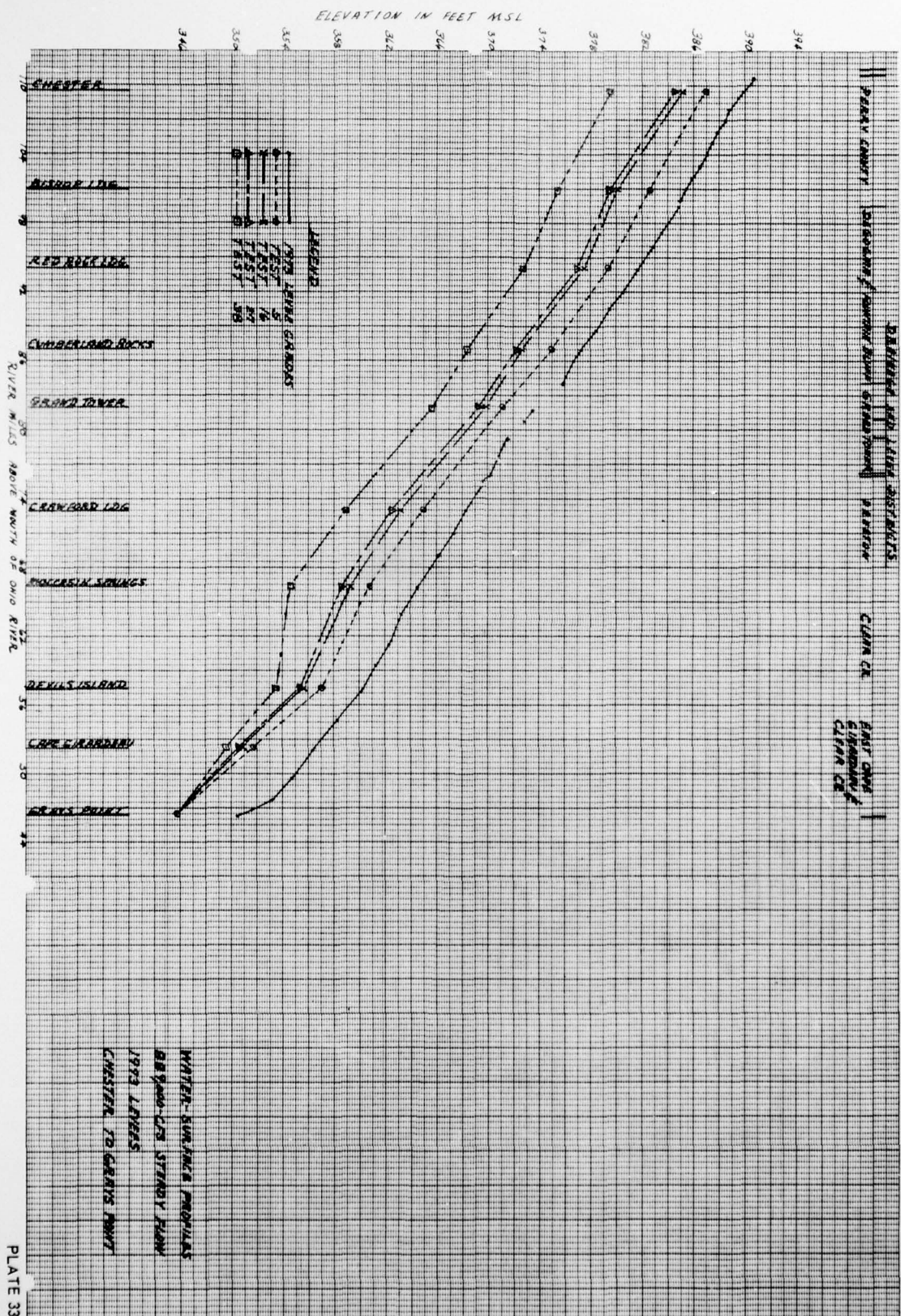


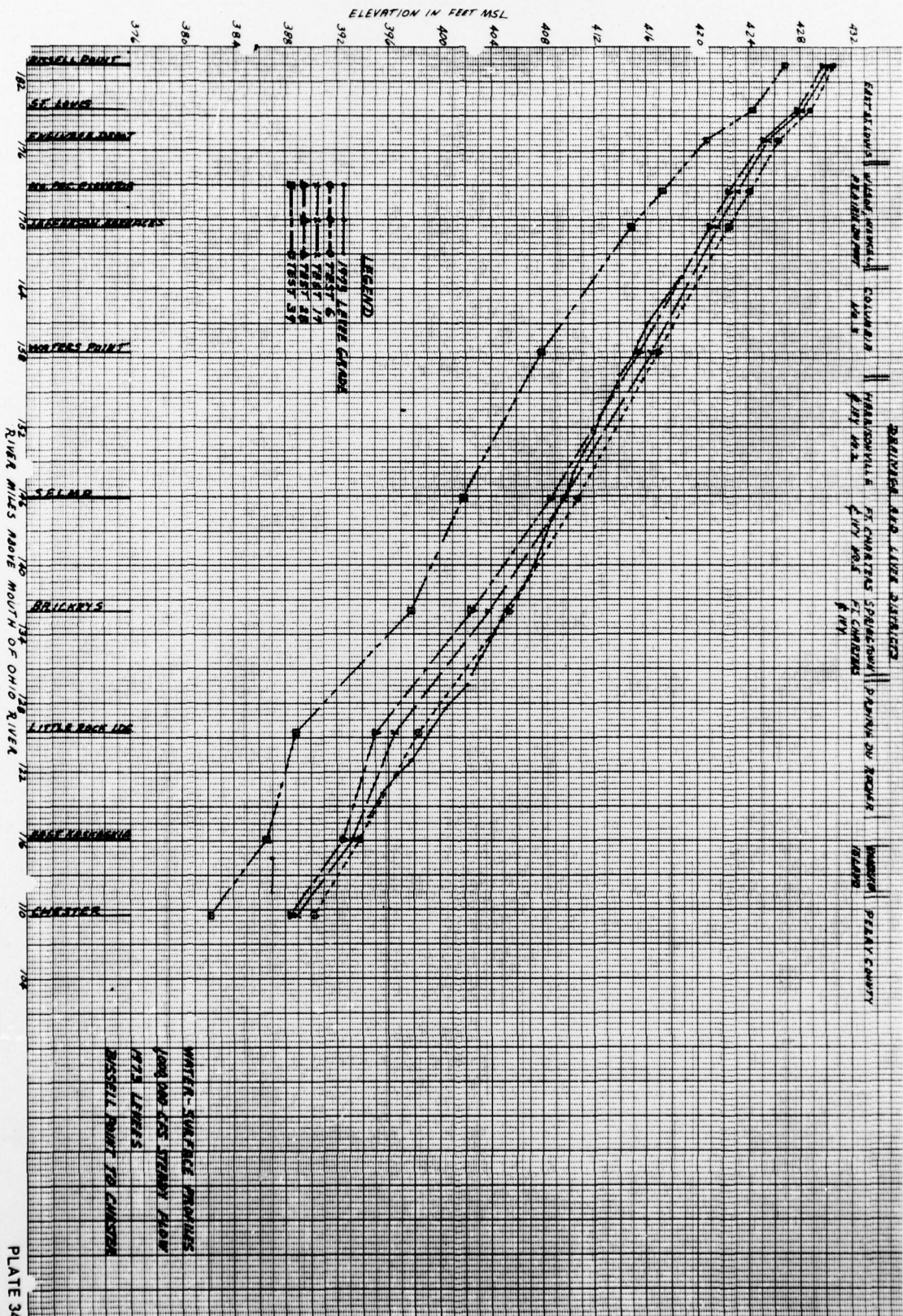


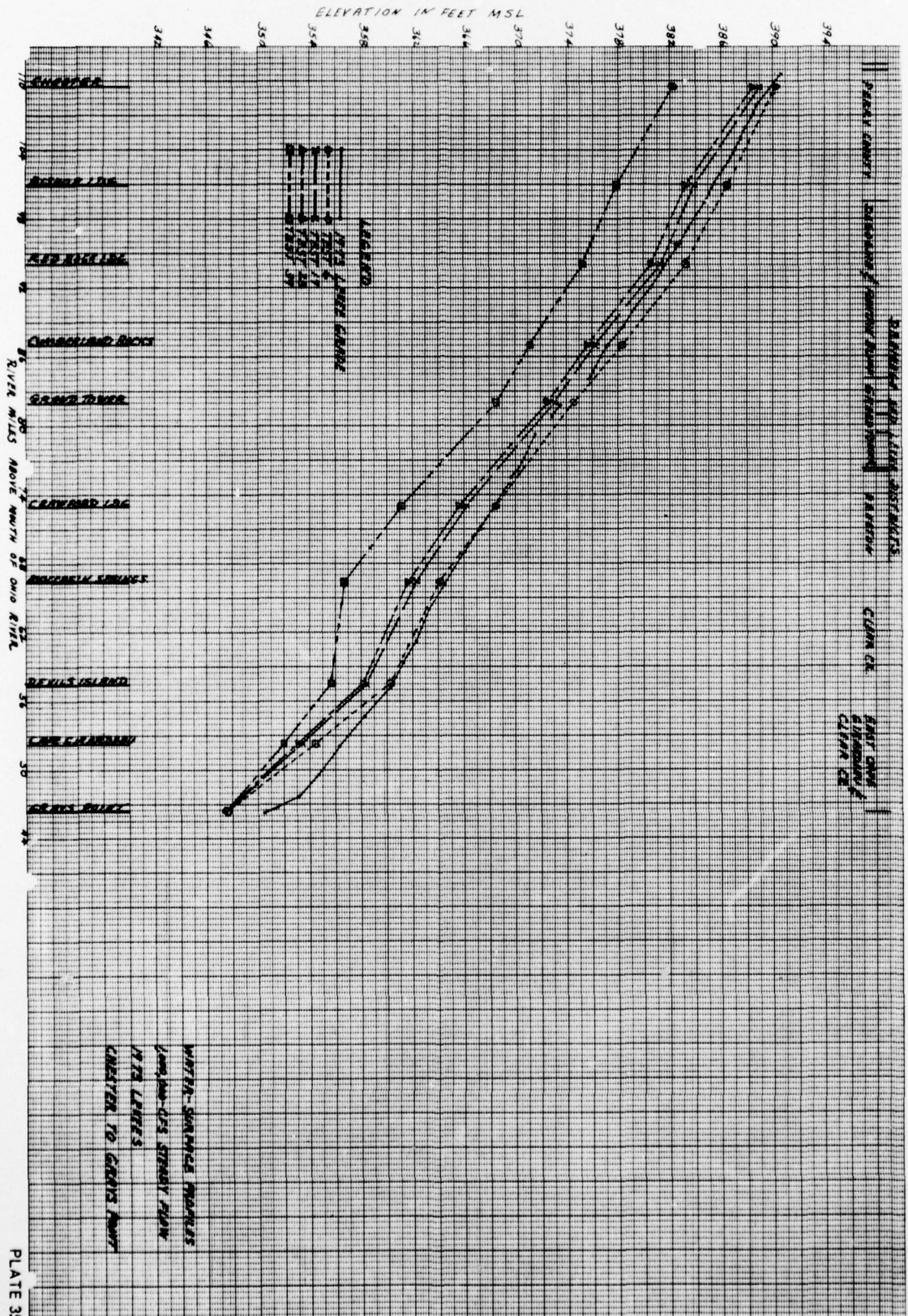


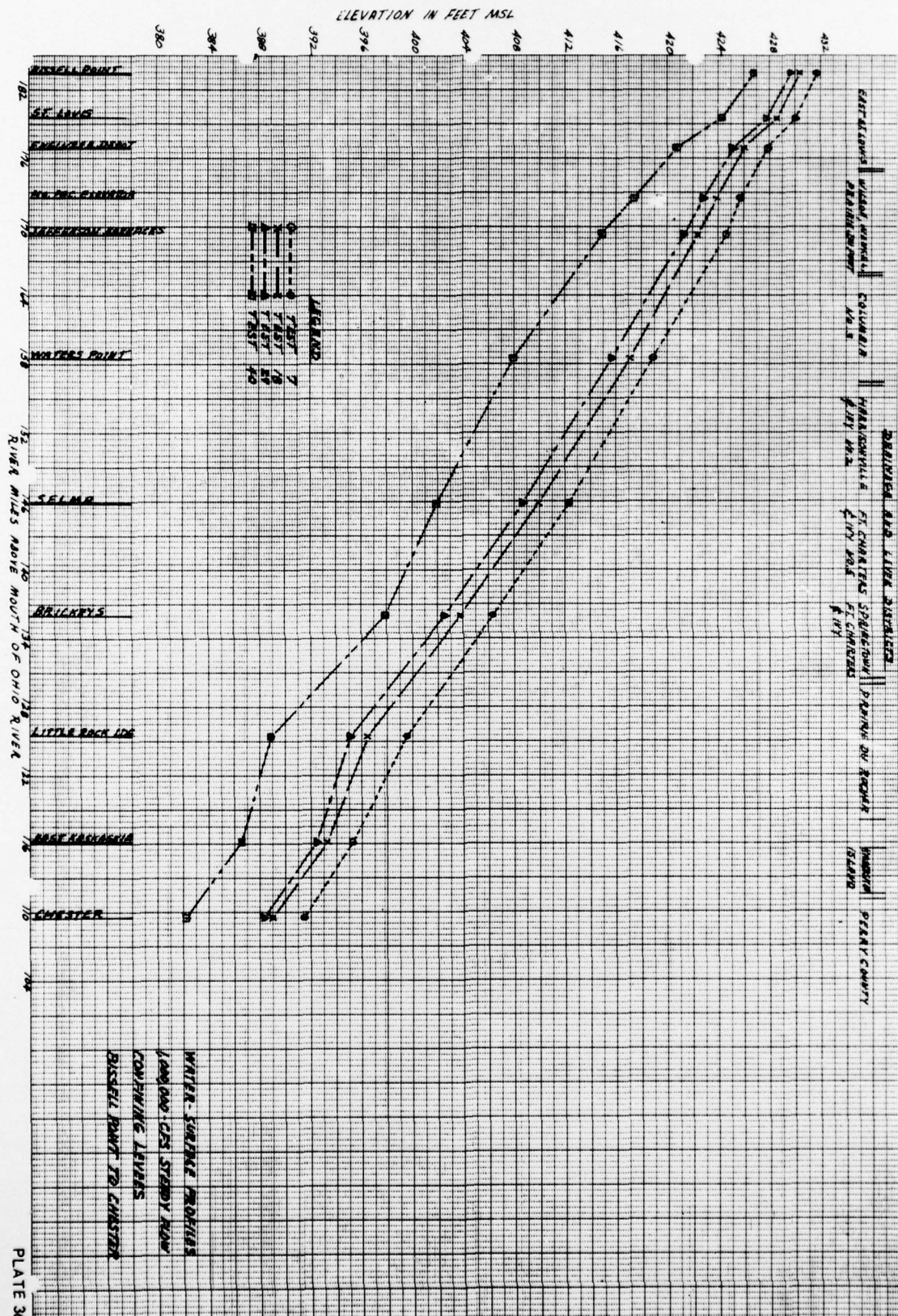


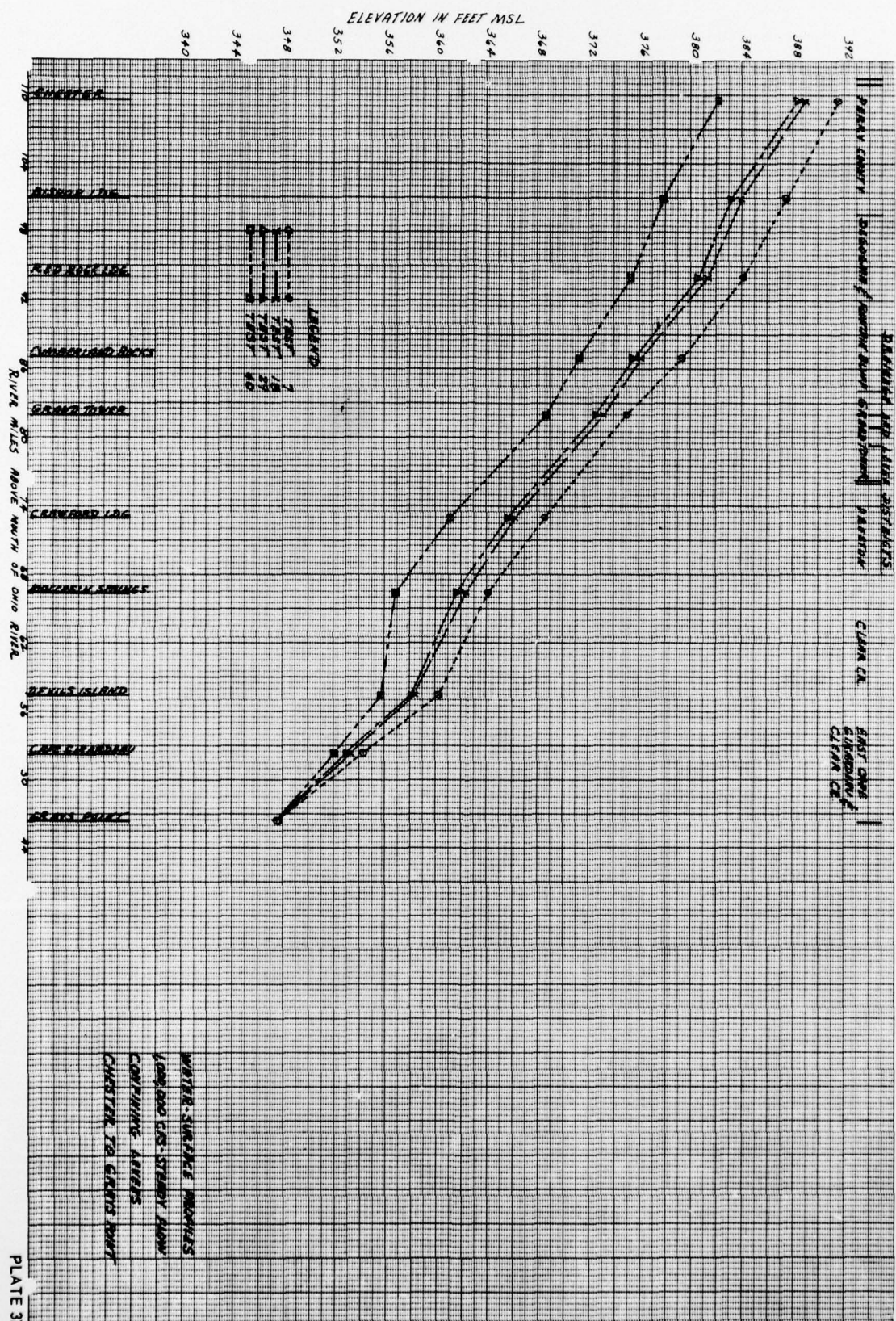


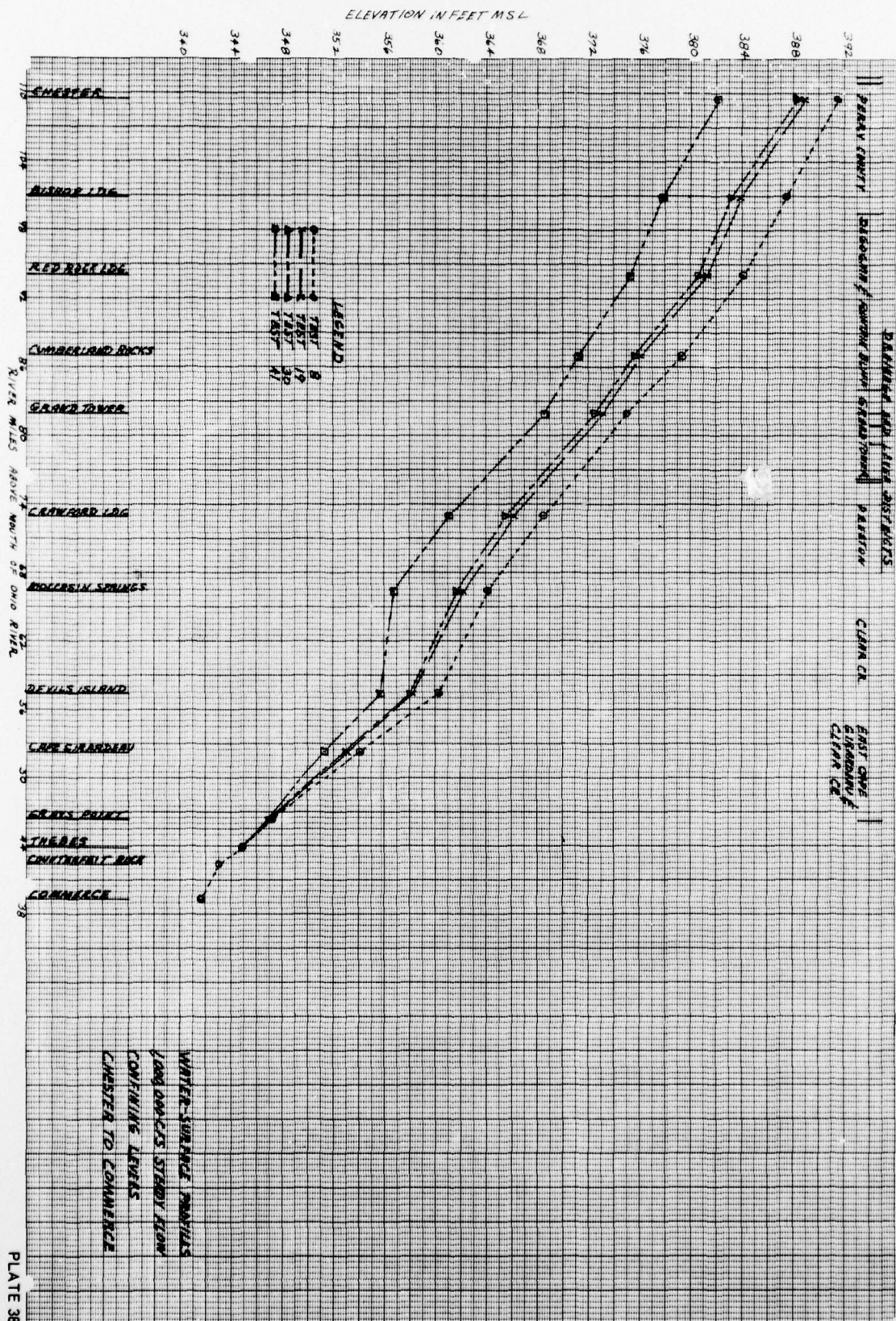


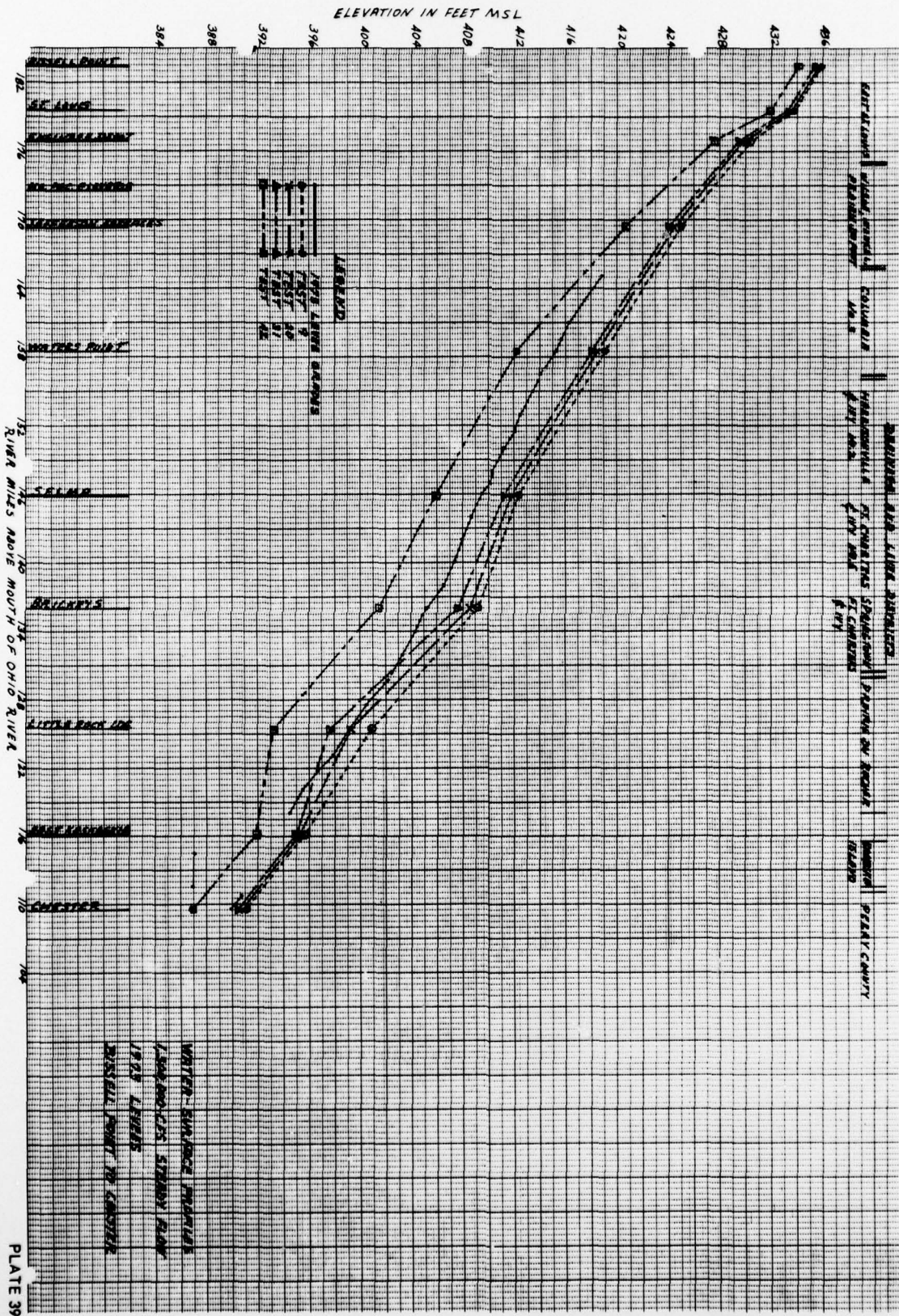


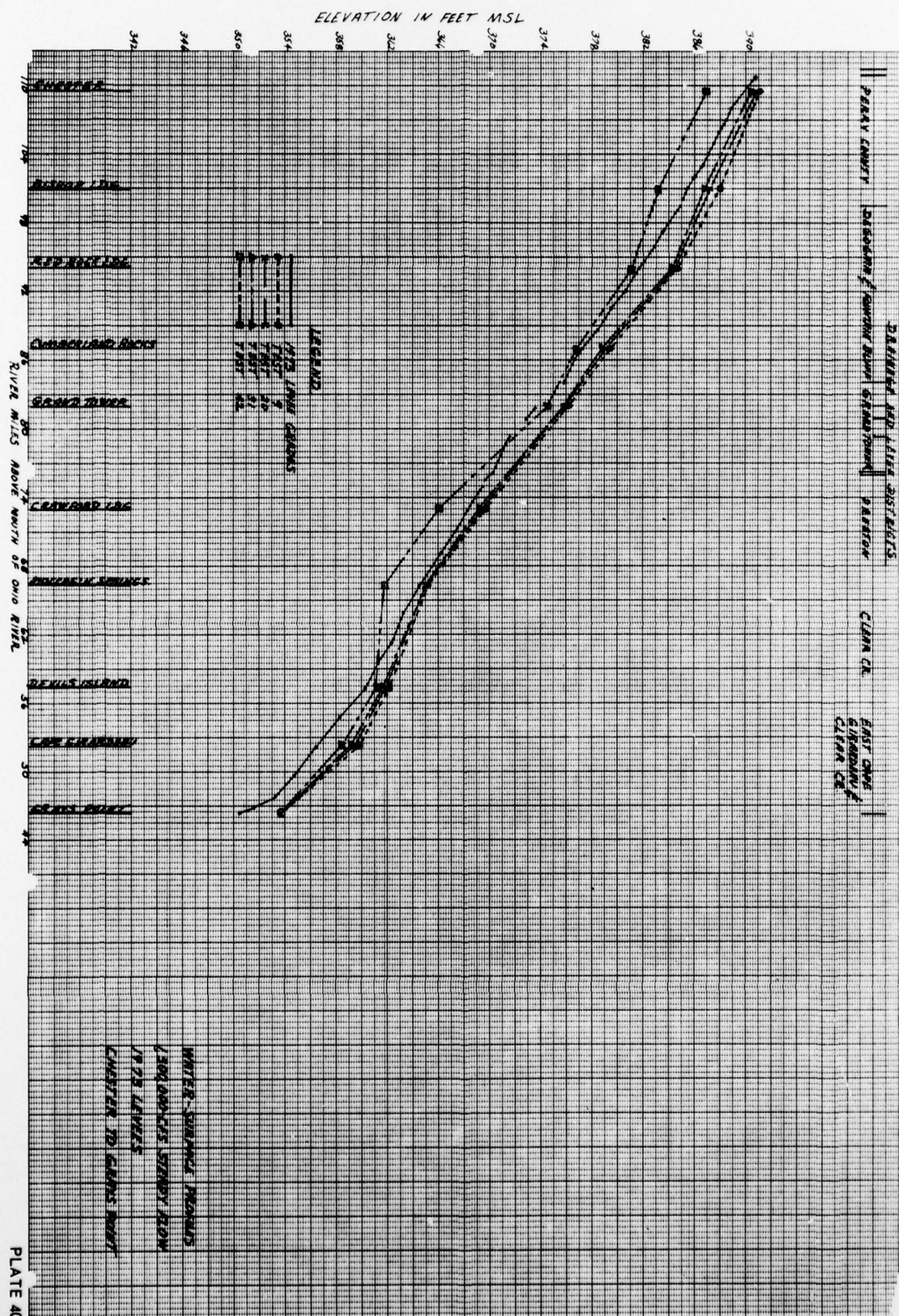


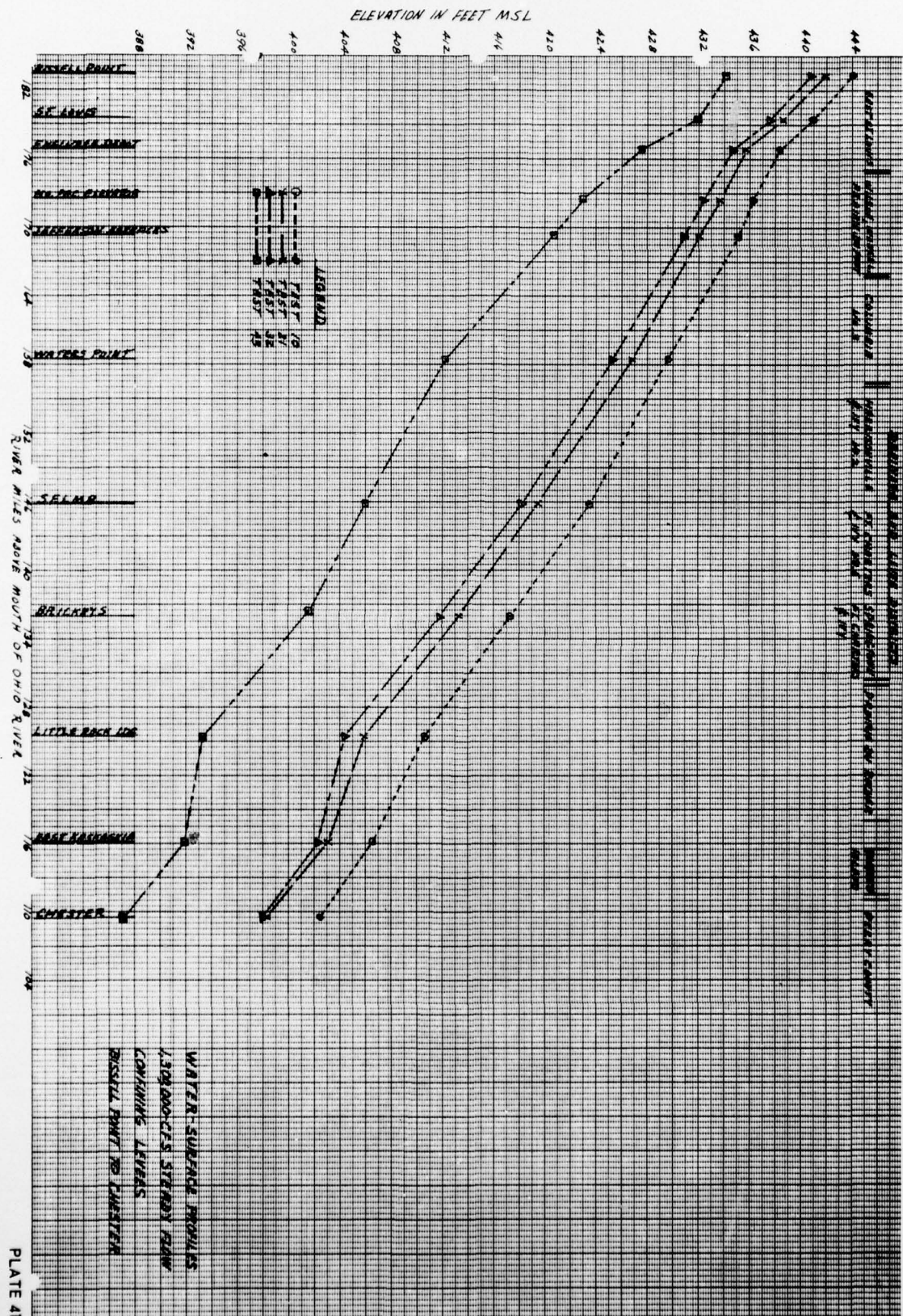


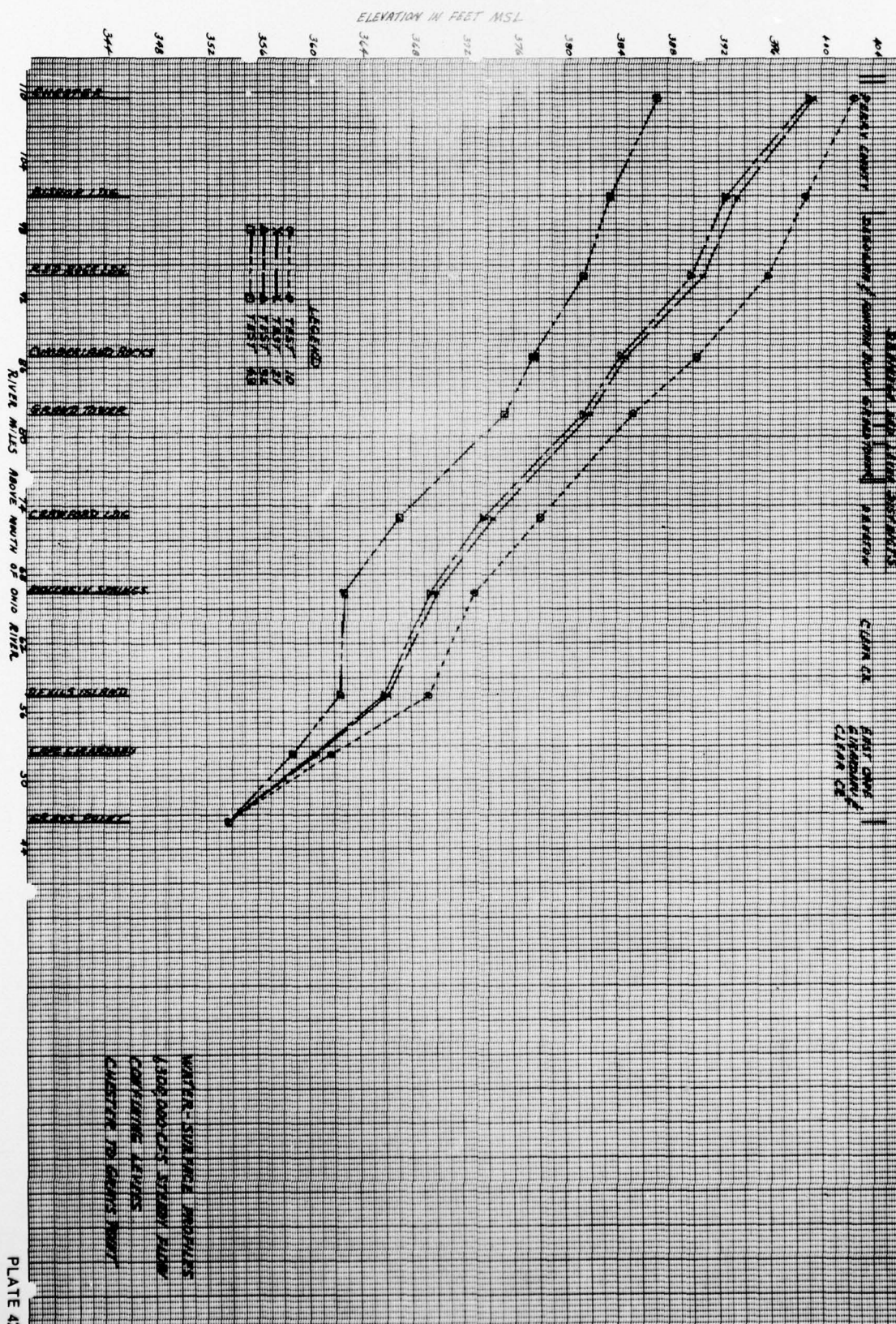


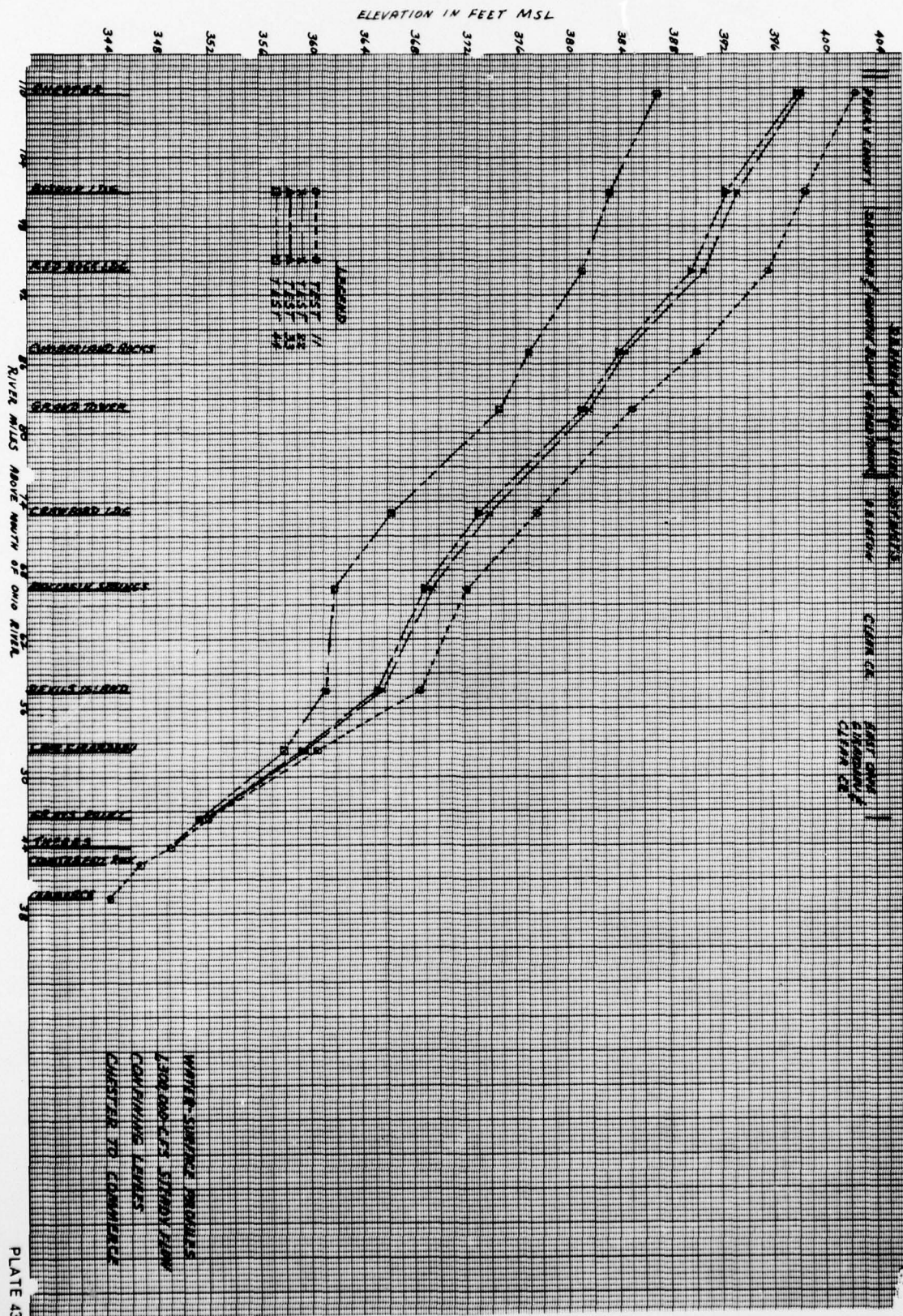












In accordance with letter from DAEN-RDC, DAEN-ASI dated 22 July 1977, Subject: Facsimile Catalog Cards for Laboratory Technical Publications, a facsimile catalog card in Library of Congress MARC format is reproduced below.

Foster, James E

Effects of overbank vegetation on Mississippi River stages in the St. Louis-to-Thebes Reach / by James E. Foster, James V. Allen. Vicksburg, Miss. : U. S. Waterways Experiment Station ; Springfield, Va. : available from National Technical Information Service, 1979.

7, [11] p., 43 leaves of plates : ill. ; 36 cm. (Mississippi basin model report - U. S. Army Engineer Waterways Experiment Station ; 81-6)

Prepared for U. S. Army Engineer District, St. Louis, St. Louis, Missouri.

1. Fixed-bed models. 2. Mississippi River. 3. Overbank flow. 4. St. Louis-to-Thebes Reach. 5. Streamflow records. 6. Vegetation. I. Allen, James V., joint author. II. United States. Army. Corps of Engineers. St. Louis District. III. Series: United States. Waterways Experiment Station, Vicksburg, Miss. Mississippi basin model report ; 81-6. TA7.W34b no.81-6

Key to Numbering of MEM Reports*

Test of Report or Test	Office for Which Conducted									
	General	IMVD	MRD	ORD	SND	IMVD	Reserved		Outside Agencies	Basin-wide
							for	Division		
General Reports	1-series									
MEM Board Meetings	2-series									
Papers in Technical Journals	3-series									
Reserved for Future	4-series									
Reserved for Future	5-series									
Reserved for Future	6-series									
Reserved for Future	7-series									
Reserved for Future	8-series									
Reserved for Future	9-series									
Verification Studies	10-series	11-	12-	13-	14-	15-	16-	17-	18-	19-
Reservoir-Operation Studies	20-series	21-	22-	23-	24-	25-	26-	27-	28-	29-
Levee Studies	30-series	31-	32-	33-	34-	35-	36-	37-	38-	39-
Flood-Routing Studies	40-series	41-	42-	43-	44-	45-	46-	47-	48-	49-
Changes in Regimen	50-series	51-	52-	53-	54-	55-	56-	57-	58-	59-
Reserved for Future	60-series									
Reserved for Future	70-series	81-	82-	83-	84-	85-	86-	87-	88-	89-
Miscellaneous Studies	80-series									
Combined Purpose Studies	90-series	91-	92-	93-	94-	95-	96-	97-	98-	99-

* First digit indicates type of report or test; second digit (for 10-series and above) indicates office for which performed. Numbers following dashes indicate chronological order in respective series.

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